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FINAL FOUNDATION REPORT

COMPLETION OF
EMBANKMENT AND SPILLWAY
JOE POOL LAKE
MOUNTAIN CREEK, TEXAS



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CORPS OF ENGINEERS FORT WORTH DISTRICT, TEXAS

FINAL FOUNDATION REPORT COMPLETION OF EMBANKMENT AND SPILLWAY

JOE POOL LAKE

-BYALAN J. MARR
ENGINEERING GEOLOGY SECTION

FEBRUARY 1988

PREFACE

This report was prepared in the Geotechnical Branch, Engineering Division, Fort Worth District. The report was authored by Project Geologist, Alan J. Marr, under the supervision of the Chief of the Engineering Geology Section, Robert C. Behm, and the Chief of the Geotechnical Branch, Melvin G. Green.

District Engineers for the Fort Worth District during construction of Joe Pool Lake were Colonel Donald Palladino and Colonel Albert J. Genetti, Jr. Mr. Shigeru Fujiwara was Chief of the Engineering Division. Messrs. Gary Hames, Mel Sadler, Sam Coleman, and James Leslie, each served as Resident Engineer during consecutive periods of construction. Area Engineer during construction was Mr. James D. Leslie.

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I INTRODUCTION

- The Joe Pool Dam and Lake 1 1. Project Location and Description. project is located in southwest Dallas County near Grand Prairie, The dam is located at river mile 11.2 on Mountain Creek, a tributary to the West Fork of the Trinity River. Location of the project is shown on Plate 1. The principal features of the Joe Pool Dam and Lake Project include: (1) a rolled earth-fill embankment and dike approximately 24,340 feet long having a maximum height of 108.5 feet above streambed and a crest width of 30 feet (Figure 1); (2) a service spillway perched in the left abutment at embankment station 100+00 having a concrete uncontrolled rectangular broadcrested weir 50 feet wide (Figure 2); and (3) a 10.5-foot diameter cut-and-cover outlet works conduit controlled by two 4.75 by 10.0-foot service gates (Figure 3). An additional feature included in the project was a channel which diverted eastbound surface runoff around the spillway stilling basin. A concrete drop structure (Figure 57) was constructed in the channel to control flow velocities in the channel. A general plan of the Joe Pool project is shown on Plate 2.
- 2. <u>Construction Authority</u>. Congressional authority for the construction of Joe Pool Dam and Lake is contained in Public Works Rivers and Harbor Act, approved 27 October 1965 (Public Law 89-298)

In December 1982, Public Law 97-400 was passed by Congress which officially changed the name of the project from Lakeview Lake to Joe Pool Lake. All previously published documents, design memorandums, plans, and specifications are entitled Lakeview Lake and will be referred to under the name Lakeview Lake in this report.



Figure 1. Aerial view of Joe Pool Dam and Lake Project. (Looking southwest)

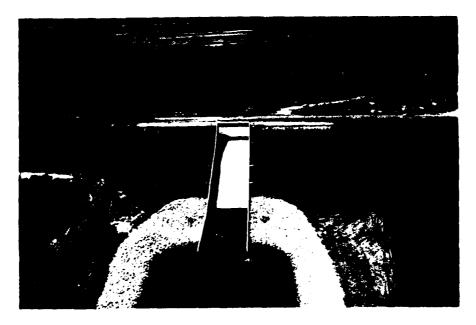


Figure 2. Spillway - Joe Pool Dam. (Looking upstream)

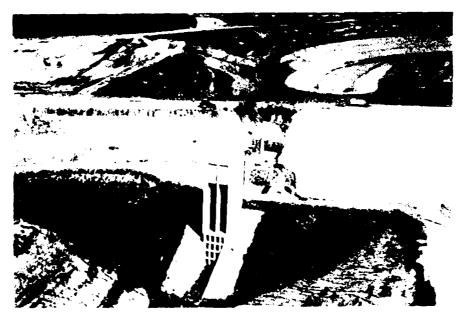


Figure 3. Outlet Works - Joe Pool Dam. (Looking downstream)

in accordance with the overall plan of improvement of the Trinity River Basin, Texas, as outlined in House Document No. 276 (89th Congress, 1st Session).

3. Purpose of the Report. This report was prepared in accordance with requirements as set forth by the Office, Chief of Engineers in ER 1110-1-1801. This is the second of two reports recording the foundation history of the appurtenant structural features of the Joe Pool project. The subject of this report is the embankment and spillway features of the project. The outlet works portion of the project was addressed in THE JOE POOL LAKE OUTLET WORKS FINAL FOUNDATION REPORT published in June 1983.

The purpose of this report is to provide a complete record of foundation conditions encountered during construction. Information contained in this report will be valuable when evaluating (1) necessary remedial action required to prevent or repair any problems resulting from foundation deficiencies; (2) contractor claims related to foundation conditions or alleged change of condition; and (3) planning and design of future comparable construction projects.

A copy of this report should be included in the permanent records maintained at the project office.

4. **Project History**. The Project Document Plan (House Document No. 276, 89th Congress, 1st Session) recommended the construction of the project at river mile 7.2 on Mountain Creek. However, upon initiation of advance planning studies for the project, it was found

that the Texas Highway Department had acquired land for the development of Interstate Highway 20 crossing Mountain Creek about one-half mile upstream from the site. The decision was made to move the dam site upstream from the interstate highway in order to avoid construction of a bridge or a costly relocation. Beginning in 1960, seven dam site locations were studied including four of them with foundation boring programs.

Fort Worth District submitted Design Memorandum No. 4 - General in December 1969 which established the location of the project at river mile 11.2 on Mountain Creek. The project plan in Design Memorandum No. 4 provided for an earthfill embankment with an uncontrolled spillway located on the right abutment at embankment station 4+30 and a cut-and-cover outlet works located at embankment station 12+25, near the right abutment. Extensive subsurface investigations at the spillway and outlet works sites revealed the presence of unfavorable subsurface geologic conditions at both Deep excavations would be required through unstable bedrock, necessitating the design of very flat excavation slopes in order to assure stability. In their review comments on Design Memorandum No. 4, it was recommended by the Office of Chief of Engineers that consideration be given to resiting the two structures. Subsequently, the Fort Worth District recommended that the structures be relocated at their present sites. In November 1978, Fort Worth submitted Design Memorandum No. 24 - Outlet Works which located the

outlet works on the main embankment section at station 76+00. **Design Memorandum No. 9 - Embankment and Spillway**, issued in April 1980, established the location of the spillway structure on the left embankment section at its present location, station 100+00.

Construction of Joe Pool Dam and Lake commenced with the award, on 19 November 1979, of a contract for the construction of the outlet works and two partial embankments. The initial contract included a floodplain embankment to elevation 514.0 from embankment station 27+00 to station 49+00; a preload embankment to elevation 564.5 from station 95+00 to station 105+00 (spillway location); the outlet works tower and associated structures, excluding the service bridge; and portions of the outlet works approach and discharge channels. Work was completed on this contract on 4 June 1982.

On 30 September 1981, Fort Worth District awarded the contract for completion of the project. Major work included in the completion contract included completion of the earthfill embankment, construction of the outlet works service bridge, construction of the spillway, and construction of the roadway atop the embankment. Other work included in this contract was the construction of the drop structure near the spillway, and completion of the outlet works approach and discharge channels. With the exception of some turfing, work on this contract was completed in April 1986.

Impoundment of Joe Pool Lake began on 7 January 1986, with conservation pool expected to be reached sometime during 1988.

Opening of the reservoir to the public is scheduled for 1988.

5. The Contracts. Joe Pool Dam and Lake was constructed under two major contracts. The contractors and pertinent data information related to the two major construction contracts are listed below:

a. Outlet Works and Initial Embankment.

Contract No. DACW63-80-C-009

Contractor: The Lane Construction Corporation,

Meridian, CT

Bid: \$11,200,632.50

Contract Awarded: 19 November 1979
Notice to Proceed: 30 November 1979
Acknowledged: 6 December 1979
Work Commenced: 7 December 1979
Work Completed: 4 June 1982

b. Completion of Embankment, Spillway, and Outlet Works.

Contract No.: DACW63-81-C-0191

Contractor: Servidone Construction Corporation,

Castleton, NY

Bid: \$25,781,338.18 Contract Awarded: 30 September 1981

Notice to Proceed: 18 May 1982 Acknowledged: 18 May 1982 Work Commenced: 1 June 1982 Work Completed: April 1986

NOTE: A bid protest issued by one of the bidders delayed issuance of the notice to proceed until the protest was denied.

- 6. **Quality Control**. The quality control organization was furnished and compensated by the Contractor. Mr. Claude Wise was the quality control supervisor during both major contracts.
- 7. <u>Contract Supervision</u>. The Joe Pool Dam and Lake project was constructed under the immediate supervision of the District Engineer, U.S. Army Engineer District, Fort Worth, Texas. The District

Engineer's representative for administration of the contract was Mr. James D. Leslie, Area Engineer, North Texas Area Office. Field inspection was administered by the Joe Pool Project Office, which was located adjacent to the North Texas Area Office at the project site. The following personnel participated in administering the contract:

Project Engineer

Mr. Gary Hames
Mr. Mel Sadler
Mr. Sam Coleman
Mr. Bill Gibbons
(Acting Project Engineer)

November 1979 - July 1981
July 1981 - August 1982
August 1982 - October 1984

Laboratory Supervisor

Mr. Willie Hudson November 1979 - June 1982 Mr. David Hamlet June 1982 - conclusion

II FOUNDATION EXPLORATIONS

1. <u>Investigations Prior to Construction</u>. Prior to final site selection a total of seven dam sites were investigated, four by subsurface explorations. Investigations at the selected site were initiated in 1969. Approximately 500 borings were drilled at the site, ranging in depths from 10 to 200 feet. The borings consisted predominantly of 8-inch flight auger, 6-inch Densison barrel, and 6-inch core. Several 3-inch fishtail borings were drilled for geophysical logging surveys to assess the presence and trends of structural features. Three 36-inch calyx holes were drilled at the right abutment. Ground-water levels were monitored at many of the boring locations by installing slotted plastic (PVC) casing in the boreholes.

Two spillway and outlet works sites were explored. Extensive subsurface explorations at the original sites of the spillway and outlet works on the right abutment revealed the presence of unsuitable geologic conditions. As a result of the investigations, it was determined that the two structures should not be located on the right abutment. Additional investigations resulted in the spillway and outlet works being resited at their present locations. Foundation boring locations are shown on Plates 4 through 7. Detailed logs of borings are presented on Plates 36 through 73.

2. Investigations During Construction. No unanticipated foundation

conditions or problems were encountered during construction.

Therefore, no additional investigations were required.

III GEOLOGY

1. Physiography and Regional Geology. The Joe Pool Dam and Lake project is located at the eastern edge of the Eagle Ford Prairie section of the Gulf Coastal Plain physiographic province. The dam site is characterized topographically by a moderately steep east (right) abutment, a relatively flat 5,000 feet-wide floodplain, and a gently sloping west (left) abutment.

A major topographic feature of the area is the White Rock escarpment located about one-half mile east of the right abutment of the dam. This north-northeast trending escarpment marks the easternmost limit of the Mountain Creek drainage area. Immediately west of the White Rock escarpment are numerous remnants of a small cuesta formed by a resistant limestone bed in the Eagle Ford Formation. The cuesta was subsequently eroded into a series of subrounded hills or remnants rising 30-60 feet above the present Mountain Creek valley. One of these hills forms the dam's moderately steep east abutment, while other similar remnants generally form the eastern shore of the reservoir area. Low, gently rolling topography forms the western boundary of the reservoir area.

Bedrock strata underlying the embankment and reservoir area consist of Upper Cretaceous units of the Eagle Ford Formation. The regional structure of these beds is monoclinal, resulting in a gentle dip southeastward toward the Gulf Coast. The maximum thickness of the Eagle Ford Formation at the dam site is 225 feet as indicated by

borings along the dam axis which penetrated the Eagle Ford to the underlying Woodbine Formation. Lithologically the Eagle Ford Formation consists predominantly of soft to moderately hard clay shale. An areal geology map is presented on Plate 3.

2. Geology of the Dam Site.

Description of the Overburden. Overburden consisting of Quatermary age alluvial and terrace deposits cover all bedrock at the dam site with the exception of some isolated areas on the right abutment where weathered bedrock has been exposed by hillside The deposits consist predominantly of clay, erosion. heterogeneous assortments of silt, sand, and gravel either mixed in or occurring separately. Overburden materials encountered during preconstruction investigations and observed during construction in the shallow inspection trench were predominantly clays, sandy clays, and gravelly clays. Impure sand and gravel deposits are generally found near the base of the overburden unit. Along the embankment centerline the thickness of the overburden ranged from 3 feet at station 69+50 to a maximum of 55 feet in a buried stream channel at station 15+00. A geologic profile along the embankment centerline is presented on Plates 8 through 11.

Overburden deposits at the right abutment consist of 4 to 10 feet of clay, sandy clay, and gravelly clay locally cemented into a weak conglomerate. A buried stream channel is located at the base of the right abutment (Plate 13). The channel, whose bottom was about 55

feet below ground surface, at elevation 442, contained alluvium and colluvium consisting of clay with variable amounts of sand, gravel, reworked shale fragments, and chalky limestone fragments.

In the valley section of the embankment, between stations 17+00 and 65+00, the overburden consists of Recent floodplain deposits having an average thickness of 45 feet. In general, these deposits consist of 35 to 40 feet of medium to high plasticity clay underlain by 5 to 10 feet of semi-impervious clayey sand and gravel immediately overlying bedrock. Excavations within this unit in the vicinity of the old Mountain Creek channel (station 53+00 to 56+00) encountered pockets of organic materials and some water-bearing sand and gravel zones (Figures 13 and 14).

Quaternary terrace deposits mantle the bedrock from about station 65+00 to the west end of the dam. These deposits consist of sandy clay and clayey sand. Fairly clean sand with some gravel was noted from station 72+00 to 75+00 (Figure 22). This area was formerly the site of an old abandoned gravel pit. Average thickness of the terrace deposits is about 30 feet.

Plans and profiles showing the materials observed in the embankment centerline inspection trench are presented on Plates 14 through 26. Photographs of the materials exposed in the inspection trench are shown in Figures 16 through 38. Boring logs presented on Plates 36 through 73 provide detailed descriptions of overburden encountered during drilling investigations.

b. <u>Bedrock Stratigraphy</u>. Primary strata beneath the dam site belong to the Britton member of the Eagle Ford Formation, Upper Cretaceous in age. Thickness of the Eagle Ford ranges from about 80 feet at the west end of the dam to approximately 250 feet at the right abutment. Immediately underlying the Eagle Ford are the interbedded sand and clay shale strata of the Woodbine Formation.

The Britton member, which is the lowest (oldest) member of the Eagle Ford Formation, is divided into three units based on lithology. In ascending order they are: (1) the Lower Britton, Unit I; (2) the Lower Britton, Unit II; and (3) the Upper Britton. During construction of the dam, strata belonging to the Upper Britton Unit were exposed in excavations for the spillway, the diversion channel and drop structure, the outlet works, and in the deep inspection trench at the right abutment. The Lower Britton, Unit II, was exposed during excavation for the outlet works stilling basin. None of the construction excavations penetrated the Lower Britton, Unit I.

Along the embankment alignment, beds of the Upper Britton Unit lie directly beneath the overburden between stations 0+00 and 45+00, and from station 63+00 to 113+00. Overburden is supported by strata of the Lower Britton, Unit II, from station 45+00 to 63+00, and between stations 113+00 and 168+00. From station 168+00 to the west end of the embankment, overburden is underlain by beds belonging to the Lower Britton, Unit I. The bedrock units dip southeastward resulting in the older strata occurring nearer the surface

progressively westward, and the contacts between the units occurring at greater depths as they progress eastward. A geologic profile along the embankment centerline showing the bedrock stratigraphy is presented on Plates 8 through 11.

- Bedrock Lithology. All foundation excavations performed during this contract, which included excavations for the deep inspection trench, the spillway, and the drop structure, were confined to strata of the Upper Britton member of the Eagle Ford Formation. The Upper Britton consists of soft to moderately hard, slightly calcareous, highly jointed and fractured bentonitic clay shale. Unweathered Upper Britton strata varies from gray to dark gray and was generally described as thin bedded. Individual layers were usually less than I foot in thickness and often exhibited a laminated appearance. Bentonite seams observed within the Upper Britton strata were less than 1 inch in thickness, and appeared as very fine-grained, ashey, light gray to bluish gray, changing to tan soon after exposure. No where in any of the excavations were these bentonite seams prominent or continuous enough to be considered as mappable units. Scattered zones or pockets of fossil debris were found throughout the Upper Britton Unit. However, with only a few exceptions, as shown in Figure 4, the fossil fragments were unidentifiable. The strata of the Upper Britton Unit also contained scattered discontinuous limestone and claystone concretions.
 - d. Bedrock Structure. The regional structure of the Eagle Ford



Figure 4. Ammonites swallovi. Well preserved specimen observed in the exposed clay shale surface adjacent to the spillway training wall. Scattered fossil shell fragments occasionally observed in Upper Britton Formation belong to above family.

Formation is monoclinal with dip of the strata to the east-southeast at approximately 50 feet per mile. In the area of Joe Pool Lake and eastward toward Dallas, strata of the Eagle Ford Formation and the overlying Austin Chalk Formation are extensively faulted. The majority of the faults are normal faults, occurring as a result of consolidation and differential settlement of individual beds. Typical displacement across a fault line is normally less than 15 feet. Several small displacement faults were noted in the area of Joe Pool Lake, either by direct observation within excavation areas, or as inferred from preconstruction electric log interpretations and 6-inch core sample inspection. A discussion of bedrock faulting examined in the major excavation areas follows:

(1) Right Abutment Deep Inspection Trench. Subsurface investigations along the dam site centerline at the right abutment revealed that the top of bedrock dropped abruptly into the floodplain due to the erosion and cutting action of an ancient buried stream channel located at the base of the abutment. The buried channel contained a maximum of 55 feet of alluvium and colluvium consisting of clay with variable amounts of sand, gravel, shale, and limestone fragments. The right abutment was also investigated as a potential site for the outlet works and spillway structures. However, these investigations revealed the presence of a large bedrock slump block, consisting of highly jointed, fractured and brecciated shale. The slump block is located downstream of the embankment centerline in the

area where the outlet works stilling basin would be located. Rather than requiring deep excavations through unstable bedrock for the outlet works and spillway stilling basins, both structures were resited at their present locations.

As a result of these discoveries during early investigations, the decision was made to deepen the inspection trench at the right abutment so that any unstable bedrock or highly permeable channel deposits encountered could be treated and/or removed. The deep inspection trench, located between embankment stations 8+50 and 19+00, was designed to penetrate into bedrock, thus removing all pervious and semi-pervious materials from the buried stream channel. The design slopes of the trench were IV on 3H resulting in a maximum trench width of 420 feet, exposing a large surface area of bedrock for inspection. A geologic map and profile of the deep inspection trench is shown on Plate 15.

The deep inspection trench was closely inspected by geotechnical personnel from CESWF and CESWD after the bottom of the trench had reached elevation ±458, approximately 19 feet above the design excavation grade. Materials observed in the bottom of the trench consisted of unweathered clay shale of the Upper Britton member of the Eagle Ford Formation, an area of stiff, moist, brown alluvial clay, and a small pocket (less than 10 feet across) of very gravelly clay (described as colluvial material on preconstruction boring logs). The contact between the clay shale and the alluvial clay was

very distinct and vertically oriented, reflecting a buried vertical face in the bedrock which occurs at embankment centerline station 14+30. During the inspection, the decision was made to immediately terminate excavations in the deep inspection trench and start backfilling. The decision was based on the conclusion that the primary materials exposed in the floor of the trench were competent and the colluvial materials comprising the buried stream channel were sufficiently impervious so that stability and leakage through the embankment foundation would not be a problem. The material in the buried stream channel was predominantly clay and gravelly clay which would preclude excess flow beneath the dam. Although some minor faulting was present in the exposed clay shale, the bedrock generally appeared competent and in much better condition than the bedrock encountered by borings in the slump block area downstream of the embankment.

Faults that were examined in the exposed bedrock in the deep inspection trench were classified as normal faults of low displacement, generally a few feet or less. The most prominent fault crossed the embankment centerline at station 13+60 striking generally northwest, paralleling the edge of the buried stream channel. The angle of dip of the fault plane varied from 46° to 54° to the southeast and maximum vertical displacement across the fault plane was approximately 1.5 feet. A geologic map and profile of the deep inspection trench is shown on Plate 15.

(2) Spillway. The 50-foot wide spillway structure is perched in the embankment at station 100+00 on the gently sloping left abutment. The excavation for the spillway stilling basin is located at the downstream toe of the embankment. The spillway crest is founded on embankment fill. The remainder of the spillway structure rests on natural overburden and highly weathered to slightly weathered bedrock which supports the spillway stilling basin. The contact between overburden material and bedrock is located at station ll+67 on the spillway centerline. A geologic map and profile of the spillway excavation are presented on Plates 29 and 30, respectively.

Bedrock exposed in the stilling basin excavation belongs to the Upper Britton member of the Eagle Ford Formation. As predicted, some minor bedrock jointing and faulting were observed in the exposed foundation. The structural deformities in the bedrock beneath the spillway structure were predominantly classified as joints, rather than faults, because of the lack of notable displacement across the breaks. The angle of dip measured along the joints ranged from 70° to 90° (vertical). Strike of the joints was variable with an east-west direction being the dominant general trend. Jointing was more abundant within the highly weathered bedrock zones.

The bedrock strata beneath the spillway structure dips gently toward the southeast. Since there were no prominent geologic contacts, marker beds, or bentonite layers passing through the

excavation, bedding dip was most readily measured on bedding planes between the individual clay shale layers.

- e. <u>Bedrock Weathering</u>. Bedrock in various stages of weathering was encountered immediately underlying the overburden in the deep inspection trench and in the excavations for the spillway and drop structure, and the embankment inspection trench between embankment stations 65+27 and 71+00. The characteristics of the intervals of weathering can be summarized in two categories:
- (1) Highly weathered to altered. The upper zone of bedrock weathering consists of a 3- to 10-foot thick interval of residual shaley clay and clay shale weathered to a clay consistency. This zone is highly jointed, plastic, and usually moist to wet, depending on the moisture content of the overlying overburden materials. Colors of this zone are various shades of tan, brown, and gray. Where sand and/or gravel is absent, the contact between clay overburden and weathered shale can be difficult to identify.
- (2) Slightly to moderately weathered. The lower zone of weathering consists of a 5- to 20-foot thick interval of soft, tan-to-gray clay shale characterized by numerous low to high angle joints and fractures which exhibit a blocky structure. The clay shale readily breaks along the joints and fractures, but individual pieces reflect a definite shale bedding structure. Color and strength alteration is limited to zones or "halos" along the joints and fractures caused by leaching and oxidation. The boundary between

the slightly weathered zone, the highly weathered zone, and the unweathered strata below is transitional in all cases.

- f. Ground Water. Ground water is found in the semi-impervious clayey sand and gravel deposits immediately overlying bedrock throughout the valley section of the embankment. The ground water is encountered at depths of about 40 feet below the original ground surface, and the piezometric surface rises to about 20 feet below the surface. Free water was also encountered in borings in the pervious sandy strata of the Quaternary terrace deposits along the left abutment of the dam. Static water levels in this area were approximately 15 feet below the surface. A minor amount of free water was trapped in open joints and fractures in the Eagle Ford Formation; however, for the most part, the formation can be considered impervious with negligible ground-water flows. The excavations for the deep inspection trench, the spillway stilling basin, and the drop structure were entirely free of ground-water flows. No formation dewatering was required in any of the construction excavations.
- 3. Engineering Characteristics of the Overburden and Primary Materials. Engineering characteristics of the materials comprising the foundation for the Joe Pool embankment and spillway were determined by laboratory tests conducted on samples of the materials. Summaries of all laboratory test data are shown in the following publications produced by CESWF: Design Memorandum No. 24 Outlet

Works. Supplement No. 1, Initial Embankment. February 1979. (Plates 16 through 60). Design Memorandum No. 9 - Embankment and Spillway. April 1980. (Plates VI-44 through VI-62). The types of laboratory testing performed are discussed in the following paragraphs:

- a. <u>Overburden</u>. Classification tests, Q, R, and direct shear strength tests, and consolidation tests were performed on Denison barrel samples taken at varying depths. Classification and index tests were performed on jar samples taken from auger borings and Denison barrel samples. Based on field investigations, laboratory testing, and engineering judgement, the following properties were used describing overburden material units in descending order:
- (1) General overburden found on both abutments and in upper zone of floodplain overburden unit:

moisture content 21 percent dry density 107 pcf

Туре	c	0
Strength	<u>tsf</u>	Degrees
Q	1.0	1.0
R	0.3	13.0
S	0	20.0

(2) Weaker unit located just above the sand and gravel zone at the base of the overburden beneath most of the floodplain embankment:

moisture content 28 percent dry density 97 pcf

Туре	c	0
Strength	tsf	Degrees
Q	<u>tsf</u> 0.6	0
R	0.3	13.0
S	0	20.0

(3) Sand and gravel unit located at the base of the overburden beneath most of the floodplain embankment:

Туре	c	0
Strength	tsf	Degrees
S	0	30.0

b. Primary Materials. Primary materials tested included weathered and unweathered Eagle Ford shale and bentonite. Unconfined compression, Q triaxial compression, direct shear and presplit (residual) direct shear tests were performed on samples of both weathered and unweathered shale. The following properties were used for the primary materials as the design parameters:

Туре		С	0	
Material	Strength	<u>tsf</u>	Degrees	
Shale	S	0.5	18	
Bentonite	S	0	18	

IV EXCAVATION PROCEDURES

- Inspection Trench. For the purpose of describing the excavation procedures the inspection trench is divided into three areas: (a) deep inspection trench; (b) old river channel clean out; and (c) shallow inspection trench.
- a. The right abutment deep inspection trench (Figures 5 and 6) discussed earlier in this report was excavated between embankment centerline stations 8+50 and 19+00. The maximum width of the top of the trench at natural ground was 424 feet measured at station 15+00. The sides of the excavation sloped downward at a IV on 3H slope to the trench floor whose maximum width was 117 feet at station 15+00. Maximum depth of the trench was 44 feet at station 14+50. A geologic map and profile of the deep inspection trench is shown on Plate 15.

As shown on the geologic map, the trench was excavated in overburden, weathered clay shale, and unweathered clay shale, in descending order. Overburden materials in the deep inspection trench included sandy clays, clayey sands, gravels, and colluvial deposits consisting of reworked shale and limestone fragments in varying mixtures as previously described. Overburden materials were excavated and removed using Caterpiller scrapers pushed by Caterpillar D-6 and D-8 bulldozers. As the bottom of the trench descended, the IV on 3H overburden slopes were shaved and finished using motor graders. Suitable overburden materials removed from the



Figure 5. Right abutment deep inspection trench after completion of bulk excavation and prior to start of final surface cleaning and backfill. Photo taken at embankment station 8+00, looking west.



Figure 6. Right abutment deep inspection trench after completion of bulk excavation and prior to start of final surface cleaning and backfill. Photo taken at embankment station 18+00, looking east.

deep inspection trench were used as random and semicompacted fill in the embankment.

Primary material excavated from the deep inspection trench included weathered and unweathered clay shale of the Eagle Ford Formation, Upper Britton Unit (Figures 7 through 12). The weathered clay shale was excavated using methods similar to those used to excavate overburden. Excavation of the soft to moderately hard unweathered clay shale was accomplished using Caterpillar D-8 bulldozers equipped with ripper teeth. The broken material was then removed by Caterpillar scrapers. Excavation slopes in the clay shale were cut and shaved to final grade using bulldozers and motor graders. Where the slopes were smooth and even, motor graders cleaned the surface sufficiently for mapping, foundation approval, and backfill. In areas where the surface was uneven due to broken rock or ledges, cleaning by hand to remove loose material was required. A total of 161,140 yd of material was excavated from the deep inspection trench. Most of the material was suitable for use as fill in the embankment.

Ground water was not encountered in the deep inspection trench excavation, therefore, no dewatering provisions were required. The time period during which the trench was at its deepest - July thru October 1982 - was a relatively dry period with no significant rainfall events. All impervious backfill was placed on surfaces free of water.

As discussed earlier in Section III-2d, excavation in the deep inspection trench was terminated prior to reaching the design grade. Upon notification of this decision the Contractor immediately began operations for final shaving and cleaning of the excavation slopes in preparation for backfill with impervious clay. A record of approval of the exposed clay shale surfaces in the deep inspection trench is provided on Plate 34.

The former stream channel of Mountain Creek intersects the upstream toe of the embankment at station 60+50. The former channel then curves eastward and continues directly under the embankment centerline from station 57+00 to station 52+50 before curving northward and intersecting the downstream embankment toe at station 51+00. Borings indicated extensive concentrations of typical river channel deposits, including sandy, gravelly pockets and organic deposits, all of which were determined to be unsuitable as embankment foundation. The bulk of the unsuitable material was removed using Caterpillar scrapers pushed by Caterpillar D-6 and D-8 bulldozers. More saturated areas where equipment maneuverability was limited were excavated using a Caterpillar B200 track-mounted backhoe. excavation to clean out the creek channel reached a maximum depth of about 20 feet, and a maximum width of approximately 200 feet. A map of the portion of the excavation occurring beneath the embankment is presented on Plate 18. All of the material removed from this excavation was classified as overburden material; bedrock was not

encountered.

Minor ground-water flows were encountered in some of the areas of this excavation where sand and/or gravel were present. Most of the flows were isolated, and eventually dried up after they drained. Two small areas, shown on Plate 18, as A and B, continued to produce minor flow until they were covered with fill. Area B was classified as a seep, merely causing the area to remain wet, but requiring no remedial measures. In Area A, where water exited along and at the base of a slope at a rate estimated at 5 gpm, actions were taken to cut off the flow prior to placement of backfill. A 2-foot wide by ±8-foot deep ditch was cut along the top of the slope intersecting the ground-water flow. The ditch was pumped dry and immediately backfilled with impervious clay, cutting off the flow to the slope. The wet material on the slope was then removed and the area was plated and sealed with impervious clay.

c. The shallow inspection trench at the embankment centerline was excavated to a minimum depth of 5 feet below the stripped surface. Bottom width of the trench was 12 feet with IV on 1H sideslopes. The trench was excavated in intervals up to 2,000 linear feet. Excavation of the shallow inspection trench was accomplished with Caterpillar scrapers pushed by Caterpillar D-6 and D-8 bulldozers. When the trench reached the approximate required depth, the sides were cut and shaved to a IV on 1H slope using motorgraders. The scrapers were then used again to complete

excavation and removal of loose material from the bottom of the trench. The shallow inspection trench was excavated almost exclusively in overburden materials. The only exception occurred between embankment stations 65+27 and 71+00 where weathered primary material was encountered. Ground water was not encountered in the shallow inspection trench. Geologic maps and profiles along the embankment inspection trench are presented on Plates 14 through 26.

2. <u>Spillway</u>. The excavation for the spillway chute and stilling basin was located at the downstream toe of the embankment at station 100+00. The materials encountered in the excavation were described in detail in Section III of this report. Generally, the materials consisted of overburden, and weathered primary material of the Upper Britton member of the Eagle Ford Formation. The maximum depth of the spillway excavation was approximately 30 feet as measured from the stilling basin floor to natural ground. A geologic map of the spillway excavation is presented on Plate 29.

Overburden and highly weathered primary materials were excavated using Caterpillar scrapers pushed by Caterpillar D-6 and D-8 bulldozers. The excavation slopes were smoothed and shaved to IV on 3H using bulldozers and motorgraders. Slightly weathered primary materials in the lower part of the excavation were excavated by first breaking and loosening the material with a Caterpillar D-8 bulldozer equipped with ripper teeth, and then removing with scrapers. A minimum of 2 feet of undisturbed material was left above grade for

protection from damage and weathering until excavation to final grade.

Excavation to final grade around the spillway structure was accomplished with various applicable excavation equipment. evenly sloping surfaces and flat surfaces located beneath the spillway chute and stilling basin, respectively, were excavated to grade using a Caterpillar D-6 bulldozer, a John Deere 350C bulldozer, and a truck-mounted backhoe with a telescoping bucket. material was removed from the excavation using a rubber-tired front-end loader. Trenches crossing the spillway floor for the spillway drainage system were excavated using the truck-mounted backhoe, as were the footings for the spillway training walls. spillway end silland keys were excavated using a tractor-mounted backhoe. Materials adjacent to the spillway walls were excavated using the truck-mounted backhoe with telescoping bucket and the 350C bulldozer. Final cleaning of all surfaces was done by hand using compressed air and shovels. Suitable materials removed from the spillway excavation were used as random and semicompacted fill in the embankment. Ground water was encountered in the spillway excavation.

3. <u>Foundation Protection</u>. As a measure of foundation protection in the deep inspection trench and spillway, a minimum of 2 feet of undisturbed material was left in-place in areas where shale or clay shale were to be exposed at final grade. The final 2 feet was then

excavated in a continuous operation within a 2-hour period. This time limitation resulted in decreased exposure time for the surface and smaller areas being exposed at one time. The reason for this requirement was that laboratory testing and observation of the shale and clay shale materials revealed the tendency of the material to lose moisture upon exposure to air, resulting in cracking, slaking, and progressive deterioration of the material within hours of initial exposure. Additional requirements designed to limit time of exposure included requiring the first lift of fill material to be placed and compacted/sealed off within 8 hours of when excavation into the final 2 feet began or within 2 hours after achieving final grade, whichever required placement sooner.

Pneumatically placed concrete was used to seal the excavated surface on the nearly vertical walls of the spillway end sill. However, as shown in Figure 50, the first application of pneumatic concrete was unsuccessful. The concrete slumped away from the wall leaving void space and resulting in deterioration of the shale face. The contractor was required to remove the pneumatic concrete where it had slumped, achieve a fresh, undeteriorated shale surface, and reseal with pneumatic concrete. The second application was successful in protecting the shale face.

4. <u>Foundation Preparation</u>. The primary requirement for the final preparation of rock foundation surfaces prior to backfill was a thorough cleaning, which included the removal of all loose, drummy,

or deteriorated material using a combination of shovels, brooms, and blown compressed air. Backfill commenced immediately after final cleanup and approval. The strictly enforced time limitations, described above, eliminated any requirement for treatment of the exposed rock surfaces using moisture sealant spray.

There was no requirement to clean overburden surfaces by hand. Surfaces were shaved and finished with heavy equipment including scrapers and motor graders. Subsequent to inspection and approval, and prior to placement of fill, the overburden surfaces were scarified using a disc plow. Each layer of compacted impervious fill placed in the spillway and inspection trench excavations was benched in to the cut-slope on a per lift basis so that proper compaction could be performed to achieve a seal. A typical contact zone between the overburden and fill is exhibited on Figure 29.

V FOUNDATION ANCHORS

- 1. **General**. Permanent foundation anchors were installed in the spillway chute and stilling basin foundation and the drop structure foundation. A total of 214 foundation anchors were installed in the spillway and 20 in the drop structure foundation. Each was designed to extend a minimum of 15 feet into the clay shale beneath the floors of the spillway and drop structure. Plate 31 shows a plan view of the spacing of the anchors and a cross-section depicting the angle and depth of the anchors in the spillway.
- 2. Equipment. The 6-inch diameter holes for the foundation anchors were drilled using a Gardner-Denver track-mounted pneumatic drill. The anchors consisted of No. 11 rebar with a 90° bend in the top 4.67 feet and equipped with vertical bar spacers wire-fastened to the anchor for centering in the hole. A one-half inch diameter steel grout pipe designed to extend from the surface to the bottom of the anchor was permanently fixed to each anchor. The grout placed from the bottom of the hole up was delivered from an off-site source in ready-mix trucks. The following mix design was used for each truckload of grout delivered to the site:
 - 2,600 lb SSD sand 540 lb Portland cement 45 gal water
- 3. <u>Procedures.</u> Drilling and installation of the foundation anchors occurred in the drop structure during the period February-March 1983, and in the spillway April-May 1983. All of the anchors in the chute

section of the spillway were installed at an angle of 59° from horizontal; anchors in the horizontal sections of the spillway and drop structure were set at a vertical angle. Six-inch diameter holes for the anchors in the spillway were drilled through the 4-inch protective concrete slab and 12-inch sand filter blanket to a total depth of 15 feet into the Eagle Ford Shale using the pneumatic drill. Holes in the drop structure penetrated the protective slab directly into the shale - no filter was present. In the spillway, collars were fitted into the drill holes to prevent caving and loss of the sand filter. Upon completion of drilling, the holes were cleaned with air and sealed with wooden plugs. Later the holes were recleaned and the anchor bars, equipped with centralizers, were set in the holes and supported at the correct depth using wooden blocks. All holes were maintained free of water until grouting commenced. The normal procedure was to drill and plug a number of holes, insert the anchor bars, and place grout all in the same day. After the anchors were fixed in the holes at the correct elevation, the grout mixture was pumped through the one-half inch steel grout pipe until grout returned to the surface, indicating the hole was filled.

4. <u>Pull-Out Tests</u>. Prior to installation of foundation anchors in the spillway and drop structure, pull-out tests were conducted to verify the capabilities of the anchors and the foundation bedrock to withstand maximum design loads. A test was conducted on 17 January 1983, on an anchor bar in the base of the drop structure, 12 feet

left of centerline at station 8+06.5. In the spillway, a test was conducted on 15 April 1983, on an anchor bar installed 20 feet left of centerline at station 11+70 (Figure 56). The anchors were stressed to a maximum of 45 tons. Results of the tests confirmed the adequacy of the anchor lengths and hole depths specified. A detailed evaluation of the pull-out tests will be presented in the Embankment Criteria Assessment Report. Data collected during the tests are included in Appendix I.

VI CHARACTER OF THE FOUNDATION

- 1. <u>General</u>. Clay shale belonging to the Upper Britton Member of the Eagle Ford Formation, Upper Cretaceous age, comprise the rock foundations supporting the spillway structure located at embankment station 100+00, as well as the drop structure situated adjacent to the spillway discharge channel, and the main embankment in the vicinity of the right (east) abutment deep inspection trench. Overburden consisting of heterogeneous mixtures of silt, clay, sand, and gravel mantle the bedrock in thicknesses up to 55 feet. Geologic maps of the materials exposed in excavations for the spillway and the embankment inspection trench are presented in this report. Engineering characteristics of the overburden and primary materials were presented in Section III of this report.
- 2. Character of Primary Materials. Primary materials observed in excavations for the spillway, drop structure, and main embankment inspection trench consisted of slightly to highly weathered clay shale. The clay shale is generally soft to moderately hard, gray to dark gray, medium-to thin-bedded, and contains scattered pockets of fossil shells (Ammonite fragments) which are only occasionally well preserved and intact. Thin, soft to moderately hard bentonitic shale seams occur throughout the exposed sequence. Minor faulting and associated jointing and fracturing were noted in the exposed clay shale surfaces. All observed faults were normal faults, usually of

high angle and low displacement, with less than 1-foot thick brecciated zones adjacent to the fault planes. No striations were observed on the fault planes due to the softness of the rock. Joints were generally tight, occasionally calcium filled, and tended to dissipate vertically. Soon after exposure, the bedrock began to show signs of deterioration such as lightened color, hair-line cracks, and minor slaking, all due to loss of moisture. The degree of weathering of the bedrock varied from slightly weathered, where bedrock jointing had allowed penetration of iron-rich ground water resulting in orange-colored streaks described as "weathering halos" within the gray to dark gray clay shale, to highly weathered in the upper zones where exposure to ground-water leaching had literally altered the bedrock to a soft, brown to yellow clay consistency. Bedding within the clay shale suggested a slight incline toward the southeast, with occasional locally abrupt dips or flexures occurring near fault zones. Bedding thicknesses varied from a few inches to a few feet, with the individual beds separated by very thin bedding planes consisting of slightly softer, dark gray, bentonitic clay shale Excavations near the bottom of the right abutment deep seams. inspection trench encountered isolated pockets of trapped ground water which had probably percolated down through bedrock joints or faults. No actual flow was observed and the zones quickly dried up after exposure.

3. Character of Overburden Materials. Overburden materials

encountered in excavations during construction of Joe Pool Lake are described in detail in Section III of this report. The overburden consisted predominantly of clay near the surface, grading downward into sandy clay with increasing amounts of sand and gravel near the base of the overburden. Near-surface clays, as observed in the 5-foot deep inspection trench along the embankment centerline, are medium stiff to hard, silty, varying in plasticity as a function of sand content, and varying in colors as a function of the content of organic matter and minerals, specifically iron and calcium. Basal overburden exposed in excavations for the spillway, drop structure, and right abutment deep inspection trench were described as sandy to very sandy clay, occasionally very gravelly, with local areas of clayey, sandy gravel and clayey sand. Pure, clean sand or gravel was not encountered.

Minor ground-water flow from overburden materials was observed in the river channel section of the main embankment, between stations 52+00 and 57+00. No other areas of the exposed overburden produced sustained flows of ground water.

VII FOUNDATION INSTRUMENTATION

1. <u>General</u>. Instrumentation for the project consists of 18 piezometers, 3 settlement plates, 3 deep settlement plates, outlet works reference pins, and spillway reference marks. Embankment and spillway plans of instrumentation are shown on Plate 33.

2. Piezometers.

- a. <u>General</u>. Piezometers for the project were installed during both the initial and completion contracts. During the initial contract, six piezometers (P-1 through P-6) were installed. Twelve piezometers (P-7 through P-10 and P-12 through P-19) were installed during the completion contract. It was determined that P-11 would serve no useful purpose and was never installed. The piezometers installed were the porous plastic tip open tube type as manufactured by Slope Indicator Company, Seattle, Washington, with 3/8-inch diameter PVC risers.
- b. **Embankment Station 16+00**. Piezometer P-10 is founded in a sandy clayey gravel in the overburden beneath the embankment. Piezometer P-12 is founded in the unweathered clay shale beneath the overburden.
- c. **Embankment Station 38+30**, Piezometers P-1 and P-3 are founded in the unweathered Eagle Ford Shale beneath the floodplain section of the embankment. Piezometer P-3 is located in clay shale at the downstream toe. Piezometers P-2, P-4A, and P-13 are founded in sandy strata of the floodplain overburden.

- d. <u>Rmbankment Station 50+00</u>. Piezometers P-14 and P-15 are founded in a sandy clay in the overburden of the closure section of the embankment. Piezometer P-16 is founded in a gravelly clay in the overburden beneath the closure section of the embankment.
- e. **Embankment Station 63+00**. Piezometers P-17, P-18, and P-19, are all founded in the overburden of the Mountain Creek floodplain, just west of the closure section. Piezometer P-17 is founded in clay, P-18 is founded in a clayey gravel, and P-19 is founded in a sandy clay.
- f. Embankment Station 99+50. Piezometer P-5 is founded in a sandy layer in overburden and P-6 is founded in the weathered clay shale adjacent to the uncontrolled spillway.
- g. <u>Embankment Station 100+50</u>. Piezometers P-7, P-8, and P-9, are located adjacent to the spillway. Piezometer P-7 is founded in the overburden in a sandy layer. Piezometers P-8 and P-9 are founded in the weathered clay shale.
- h. <u>Conclusions from Piezometer Observations to Date</u>. The piezometers (P-1, P-2, P-12, and P-15) that have shown an increase of pore pressure, with an increase in fill height, are at the present time showing a dissipation of excess pore pressure. Only one piezometer, P-1, has shown a significant amount of excess pore pressure. Several piezometers (P-3, P-13, P-16, P-18, and P-19) are showing an increase in excess pore pressure. These piezometers are located either upstream or downstream of the embankment. This

delayed increase in excess pore pressure can probably be attributed to time lag in the response of the foundation to the load being applied. The remainder of the piezometers have either shown a small increase in pore pressure since installation (P-10 and P-14) or have not shown any excess pore pressure since installation (P-4A, P-5, P-6, P-7, P-8, P-9, and P-17).

3. Settlement and Deep Settlement Plates.

General. Three settlement plates (SP-1, SP-2, and SP-3) and three deep settlement plates (DSP-1, DSP-2, and DSP-3) were installed during the initial contract. Each settlement plate consists of a 3-foot square, one-fourth inch thick steel plate placed on the embankment foundation (top of overburden) with steel riser pipes extending through the fill. Each deep settlement plate consists of a 30-inch diameter, one-fourth inch thick steel plate placed in primary material (clay shale) with the steel riser pipes extending through the fill. The settlement plates are used to monitor the vertical movement of the entire foundation, while the deep settlement plates were used to monitor the vertical movement of the primary (clay shale) material. A plan view of the locations of the settlement plates and deep settlement plates is shown on Plate 33. These vertical movement monitoring devices were installed in essentially two locations - the floodplain and the left embankment (spillway). Results of monitoring will be discussed at each of these general locations.

- b. **Ploodplain**. Settlement Plate SP-1 (top of overburden) and deep settlement Plate DSP-1 (top of clay shale) are located below the floodplain section of the embankment at station 38+70. The foundation has consolidated a total of 1.7± feet (with 0.9± feet occurring in the overburden and 0.8± feet occurring in the unweathered primary material). The total settlement and rate of settlement achieved are well within limits that could be expected for the materials and loading involved.
- c. **Spillway**. Settlement Plate SP-2 (top of overburden) and deep settlement Plate DSP-2 (top of weathered shale) are located on the east (right) side of the spillway at station 99+50. The foundation has consolidated a total of 0.34± feet in this location (0.30± feet occurring in the overburden, and 0.04± feet occurring in the weathered and unweathered clay shale combined).

Settlement Plate SP-3 (top of overburden) and deep settlement Plate DSP-3 (top of unweathered shale) are located on the west (left) side of the spillway. The foundation has consolidated a total of 0.26± feet (0.18± feet occurring in the overburden and weathered primary combined, and 0.08± feet occurring in the unweathered clay shale).

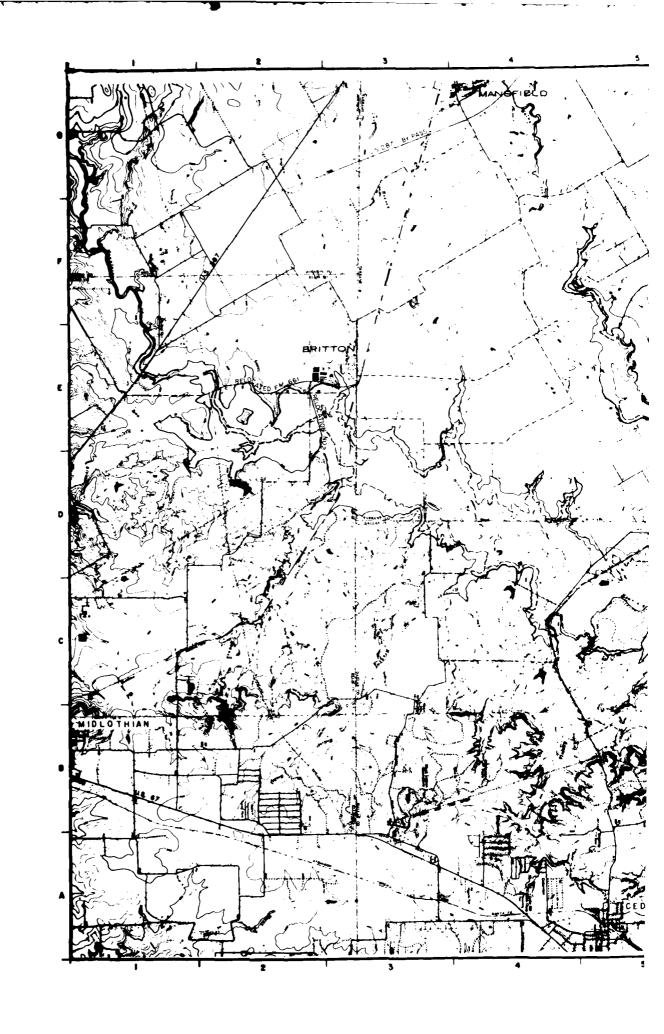
The utilization of preload initial embankment, partial excavation thereof to construct the concrete structure, and then reloading by backfilling each caused vertical movement in the form of consolidation or heave. The amount of consolidation induced due to

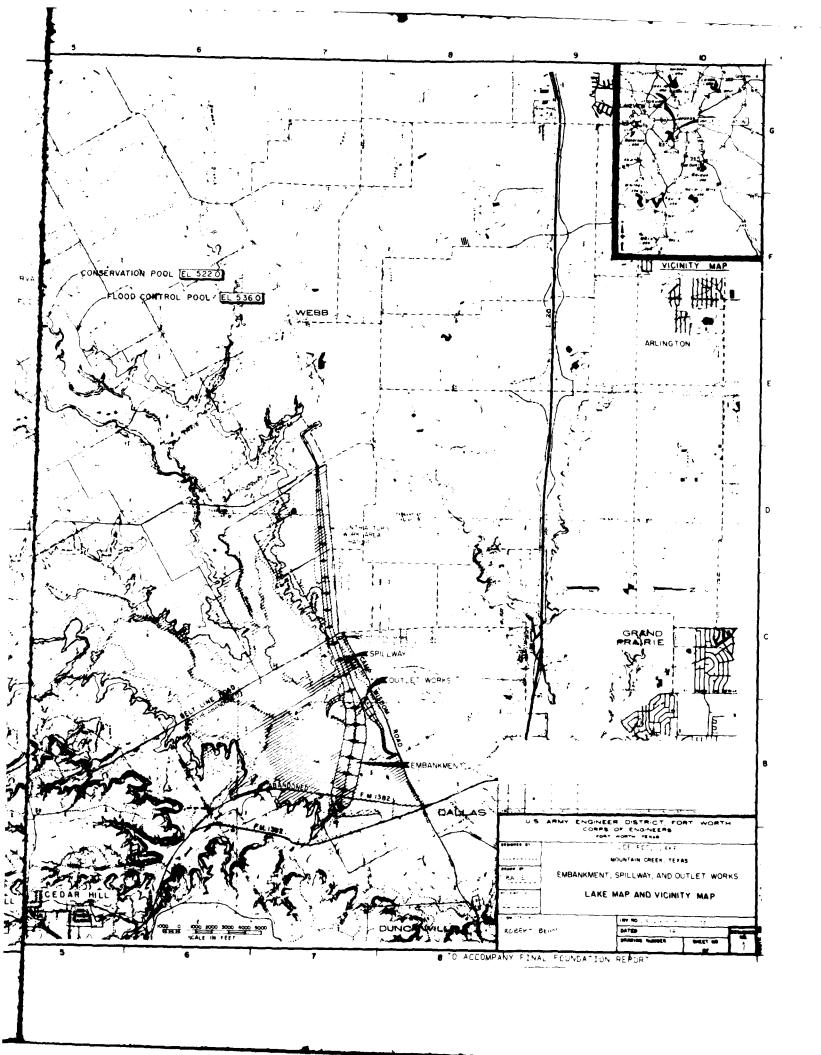
backfilling around the concrete structure is very small indicating that the preload initial embankment was very successful in its purpose of eliminating significant differential settlement at the structure.

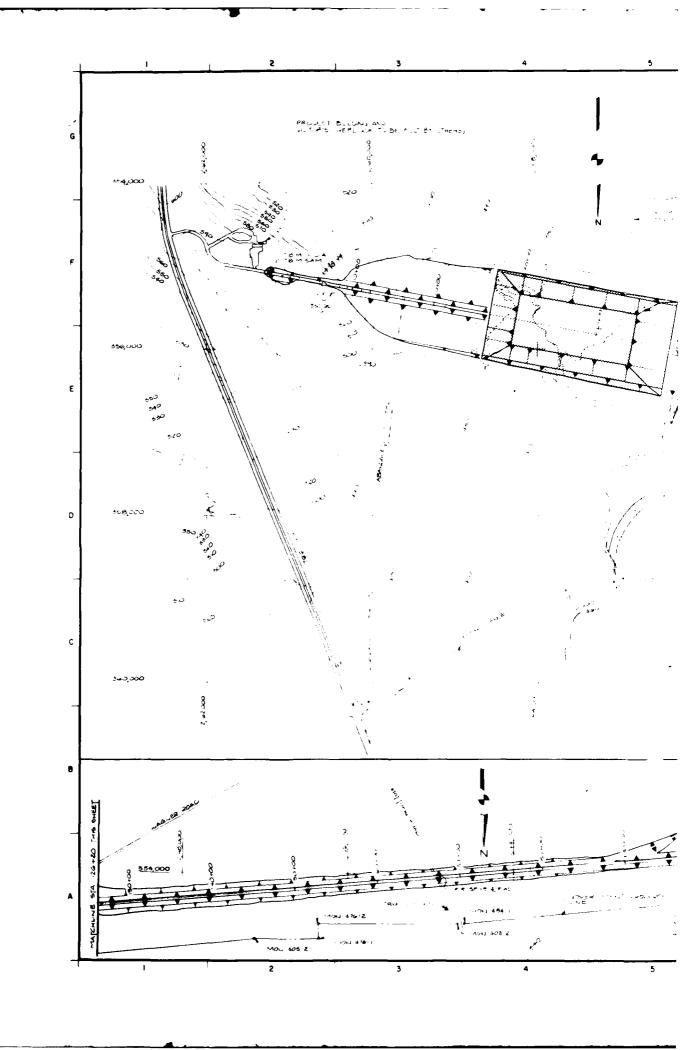
- 4. Outlet Works Reference Pins. Reference pins were installed along the invert of the conduit from the intake tower to the discharge chute, and also on the stilling basin walls. Reference pins were installed at each end of each conduit monolith, discharge chute slab, immediately downstream from the intake service gates, in the intake tower transition section immediately upstream from the first conduit monolith and on each side of each joint of both walls of the stilling basin. The reference pins consist of bronze bolts imbedded in the concrete. The surveys conducted on the reference pins show that no detectable movement has occurred in the outlet works monoliths to date.
- 5. <u>Spillway Reference Marks</u>. Reference marks were installed in the concrete of the slabs and walls of the spillway to monitor the movement of the spillway. The reference marks consist of bronze bolts imbedded in the concrete. Initial readings have been made.
- 6. **Evaluation**. The above description of foundation instrumentation was extracted from Joe Pool Lake Pre-Inspection Brochure No. 1, dated February 1986. A detailed evaluation of the foundation instrumentation program and its performance will be presented in the **Embankment Criteria Assessment Report**.

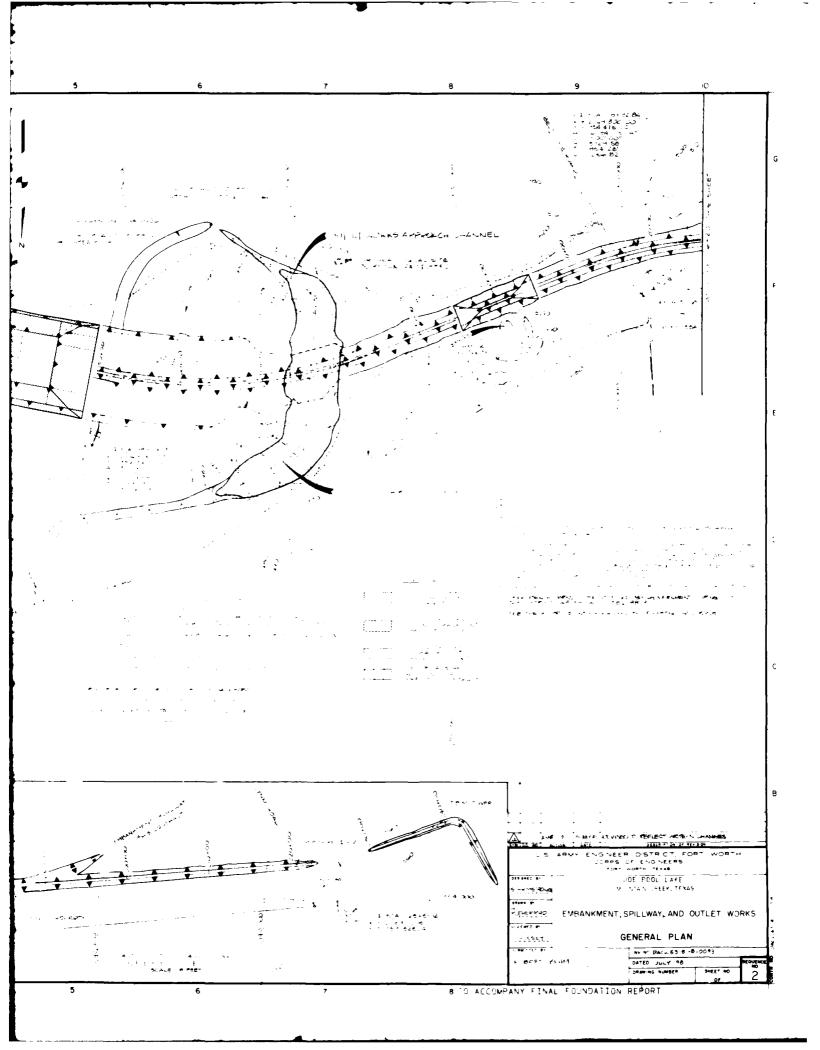
VIII FUTURE CONSIDERATIONS

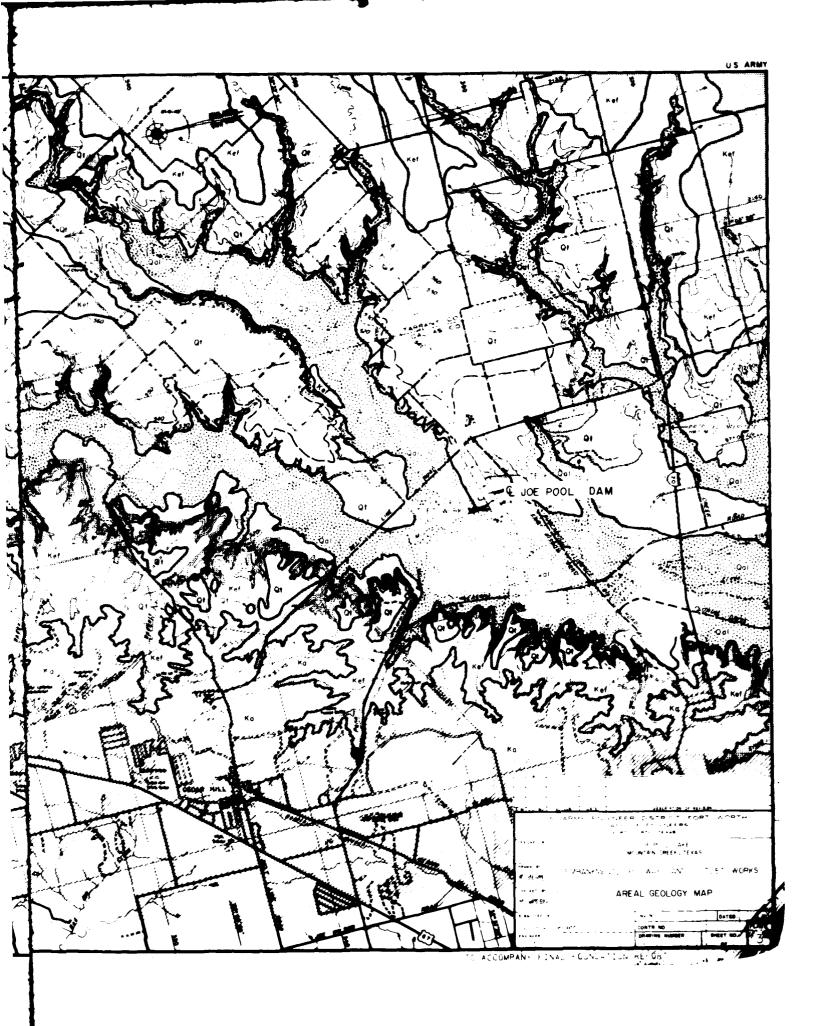
- 1. <u>Conditions That Could Cause Problems</u>. There were no unanticipated foundation conditions discovered during construction of Joe Pool Dam which would pose a threat to the stability of any of the pertinent features of the project. All bedrock surfaces were found to be competent and stable and remained so until covered by impervious backfill or protective concrete.
- 2. Recommendations. If pneumatically placed concrete is to be used for foundation protection in the future, consideration should be given to providing some type of support for the concrete when it is applied to vertical or nearly vertical slopes. When applied without support, as was the case in the spillway end sill and key trenches, the concrete tends to slump away from the slope, primarily due to its own weight, leaving a void space between the slope and the pneumatic concrete. Wire support attached to the slope and encased in the concrete would prevent this type of failure.

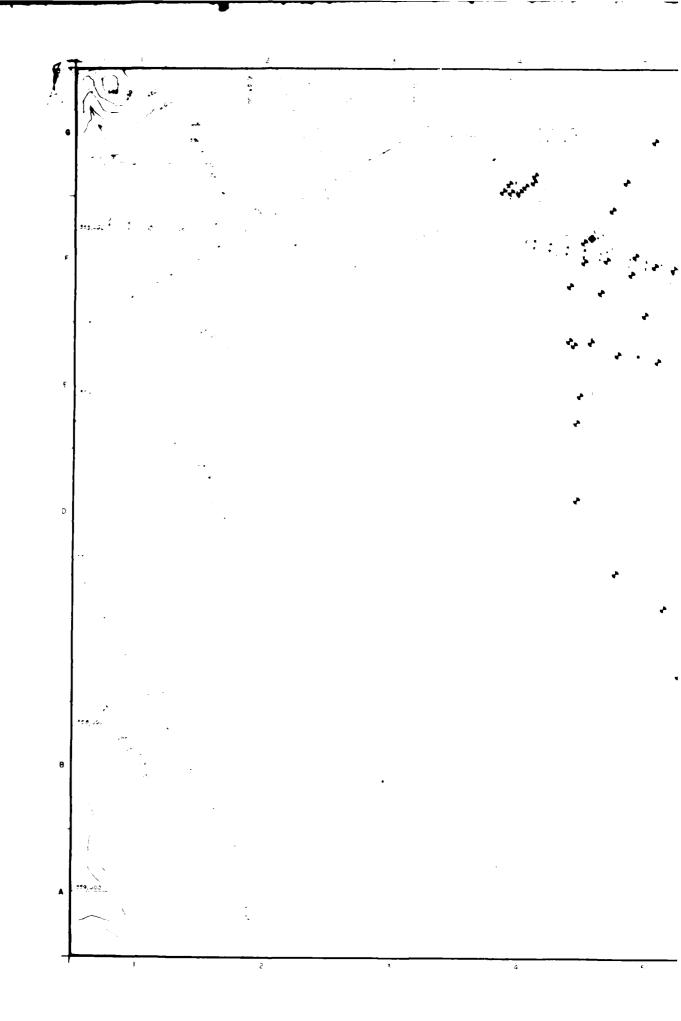


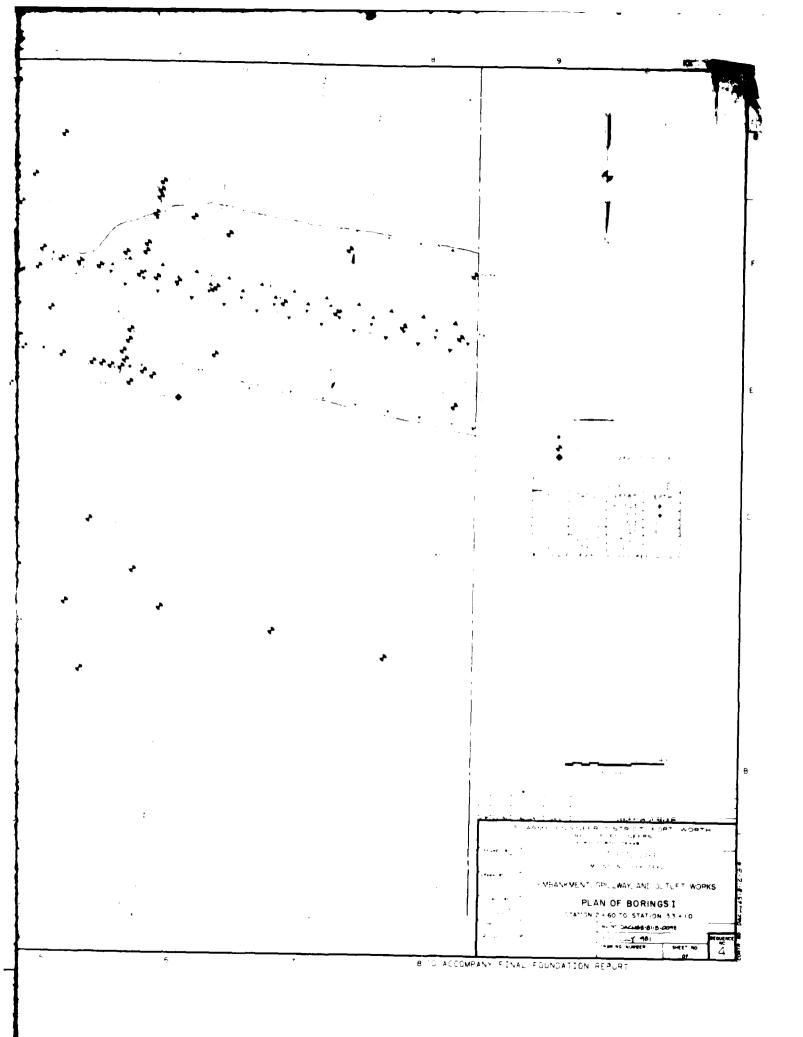


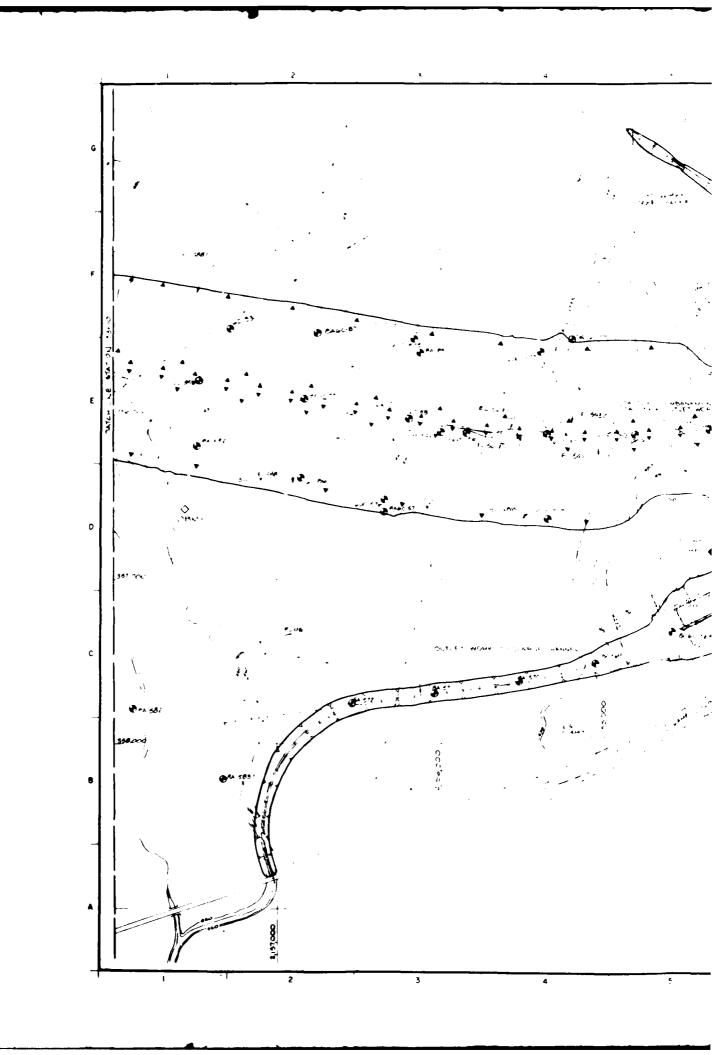


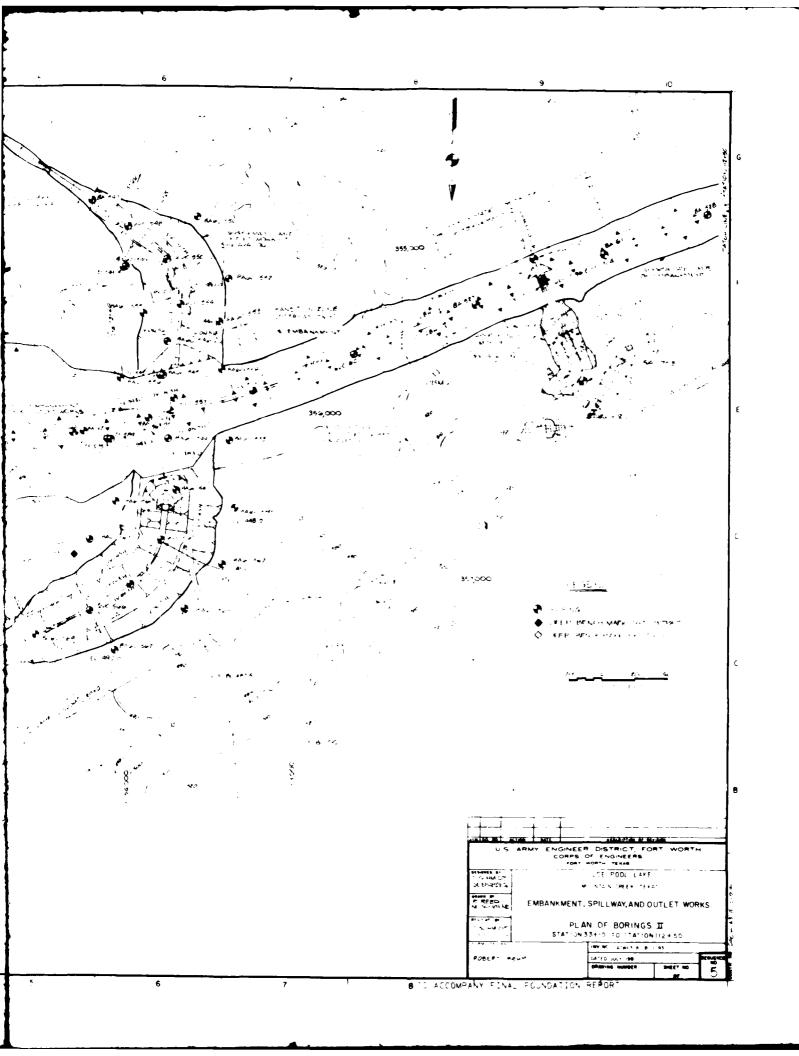


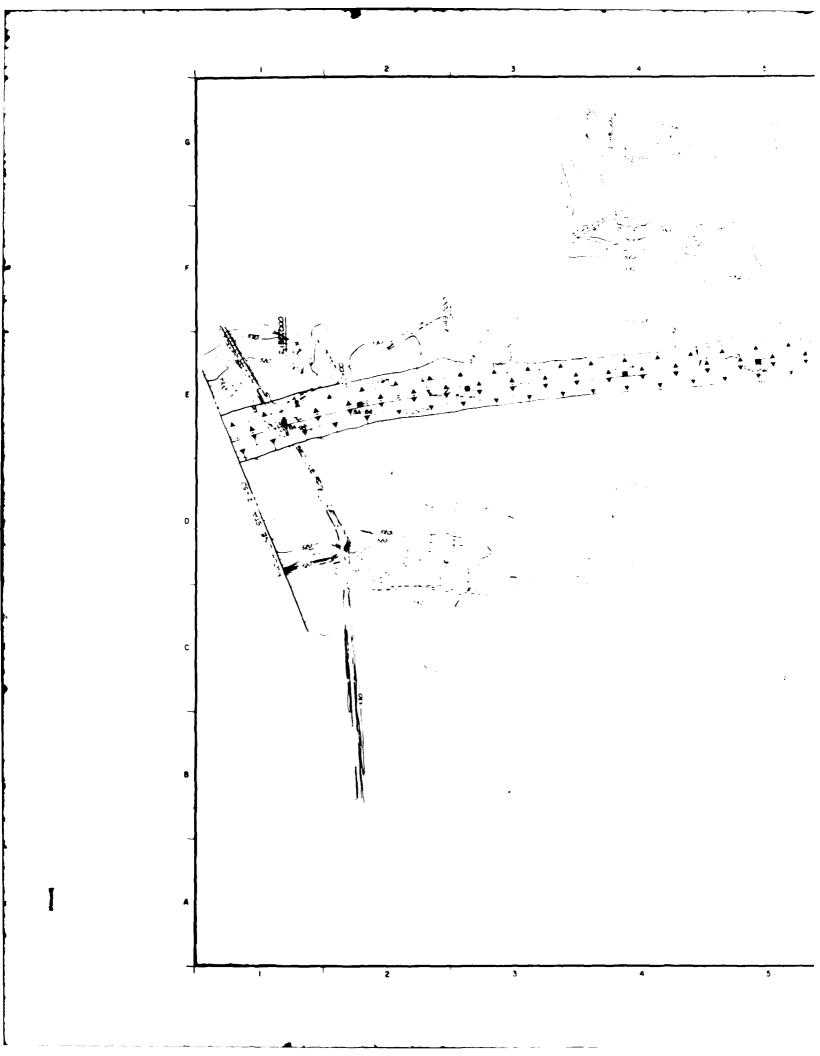












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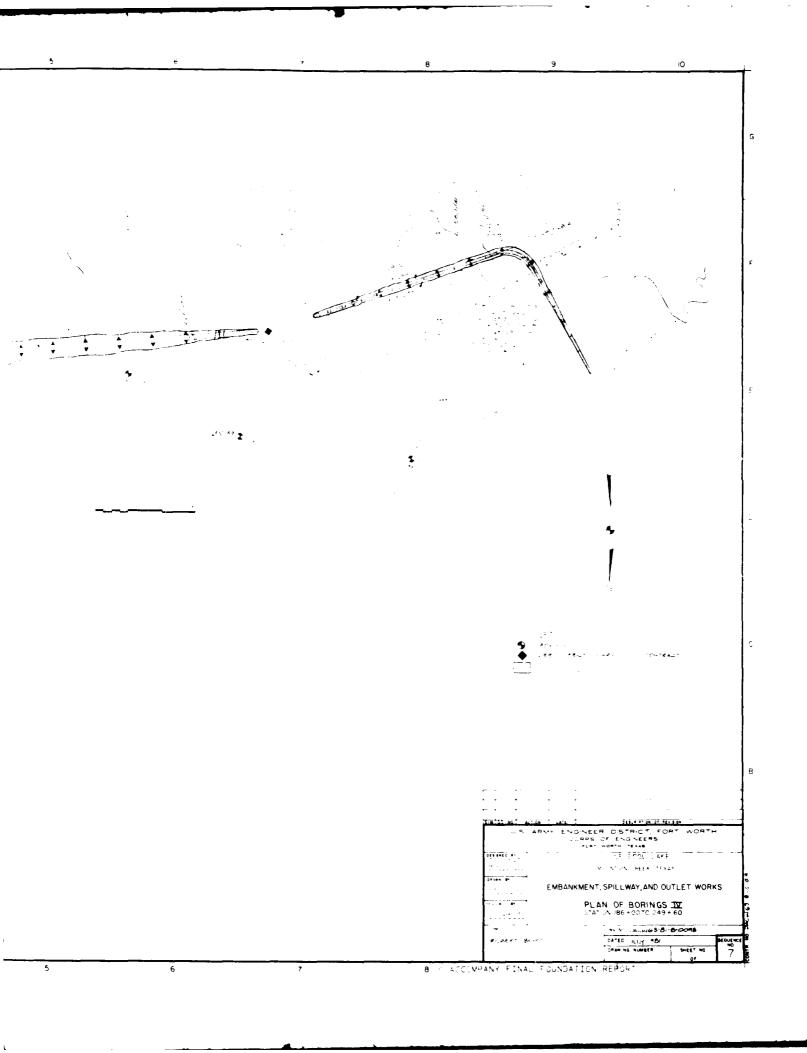
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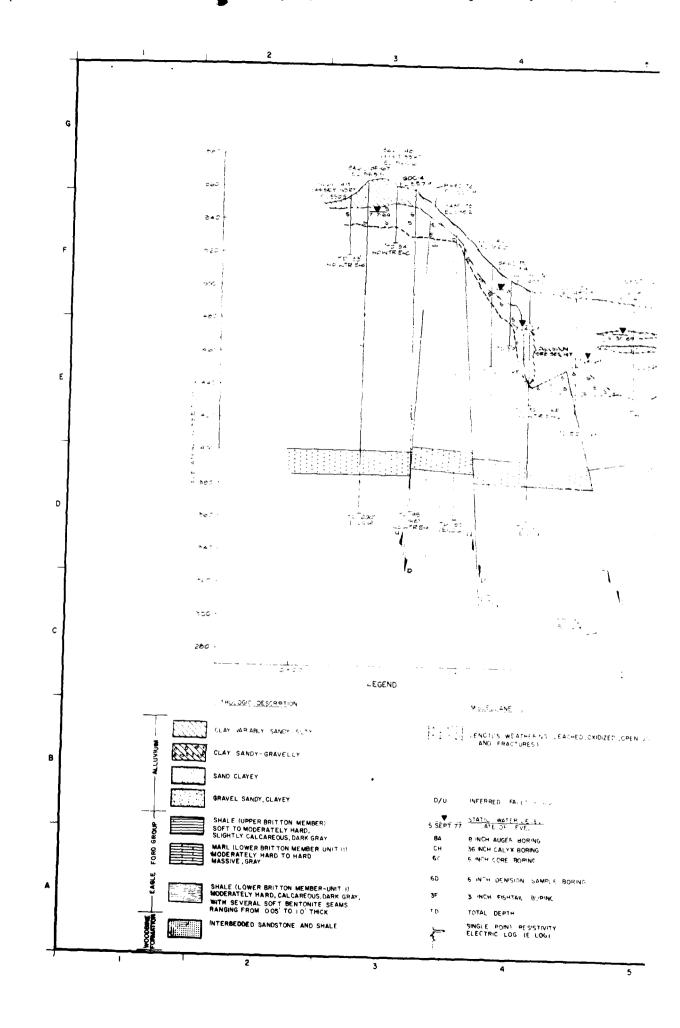
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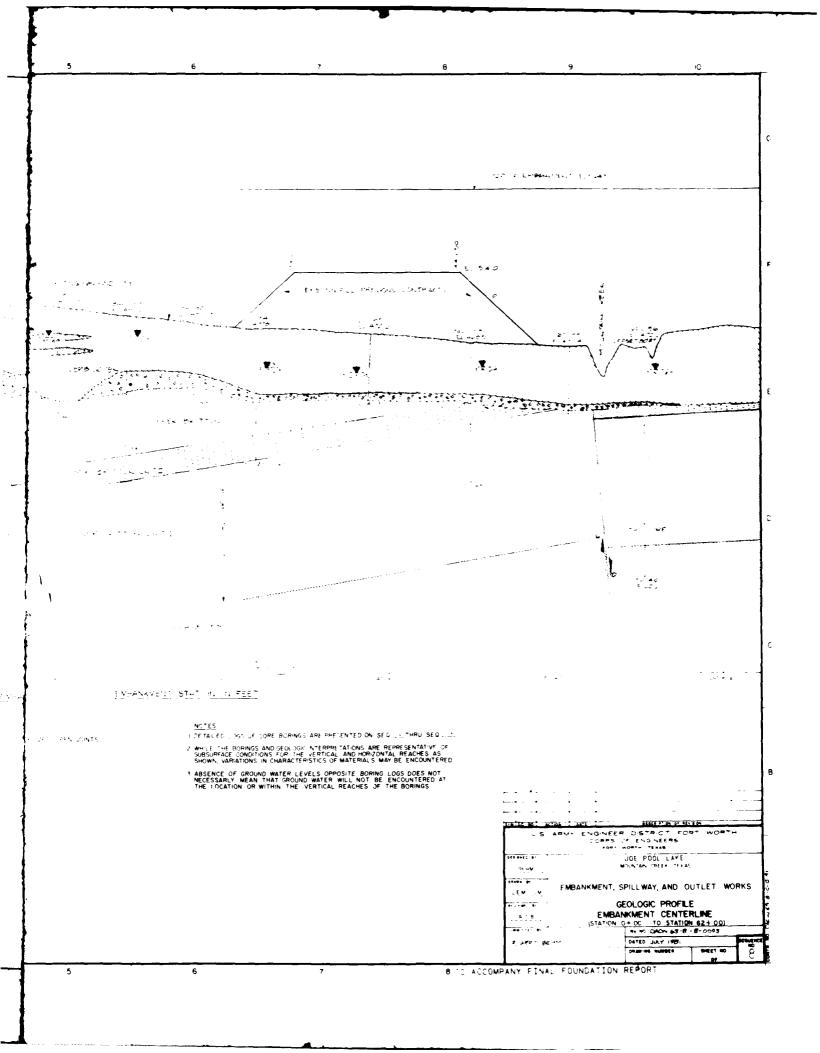
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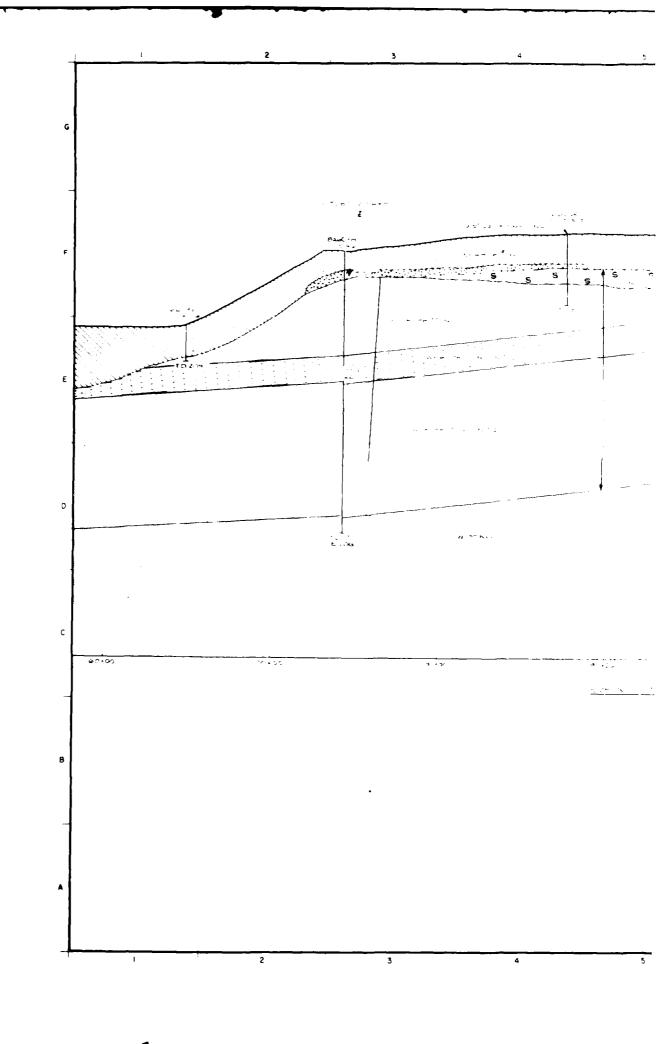
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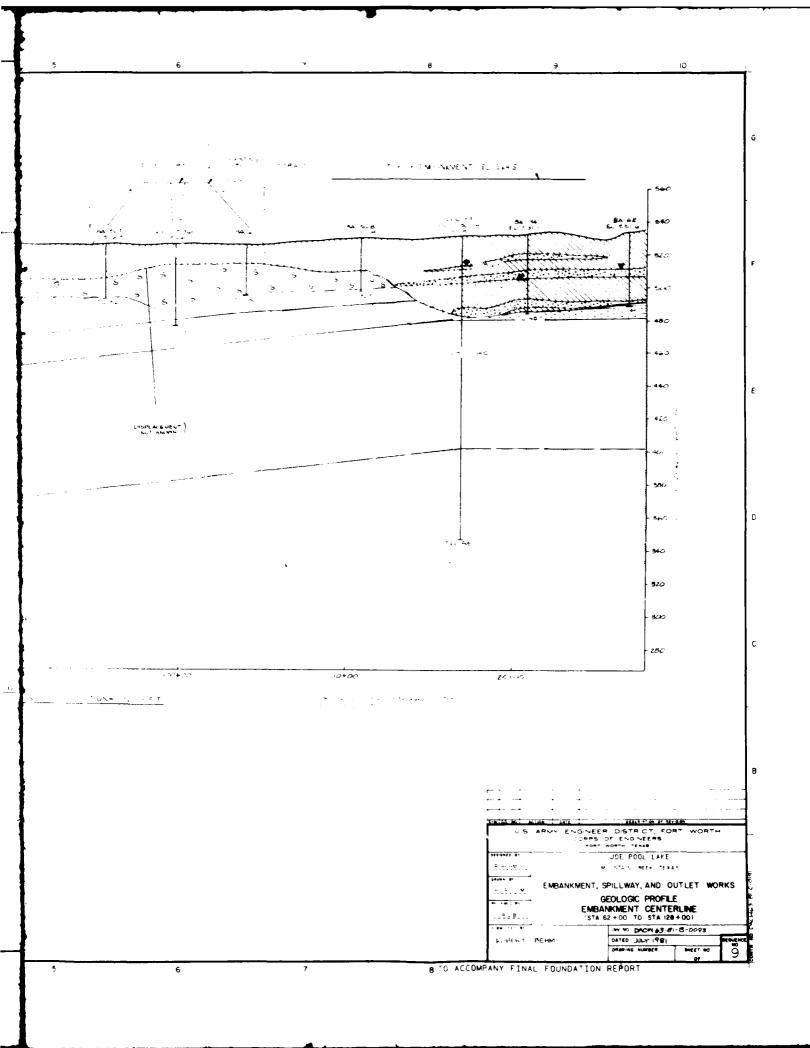
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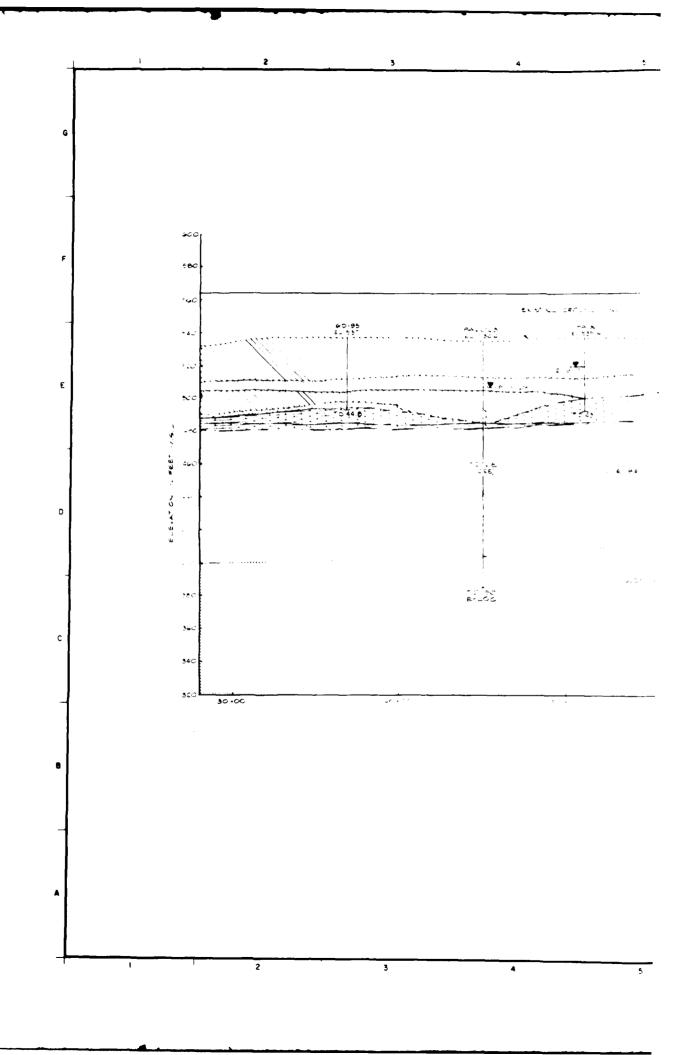








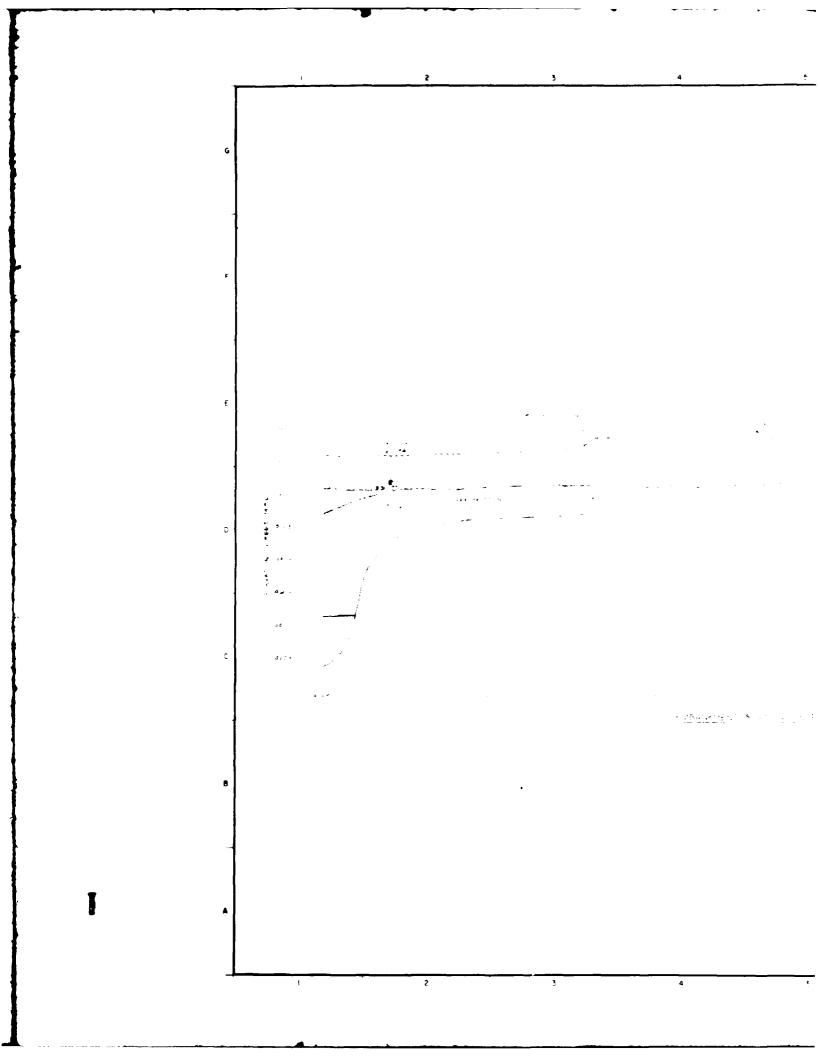




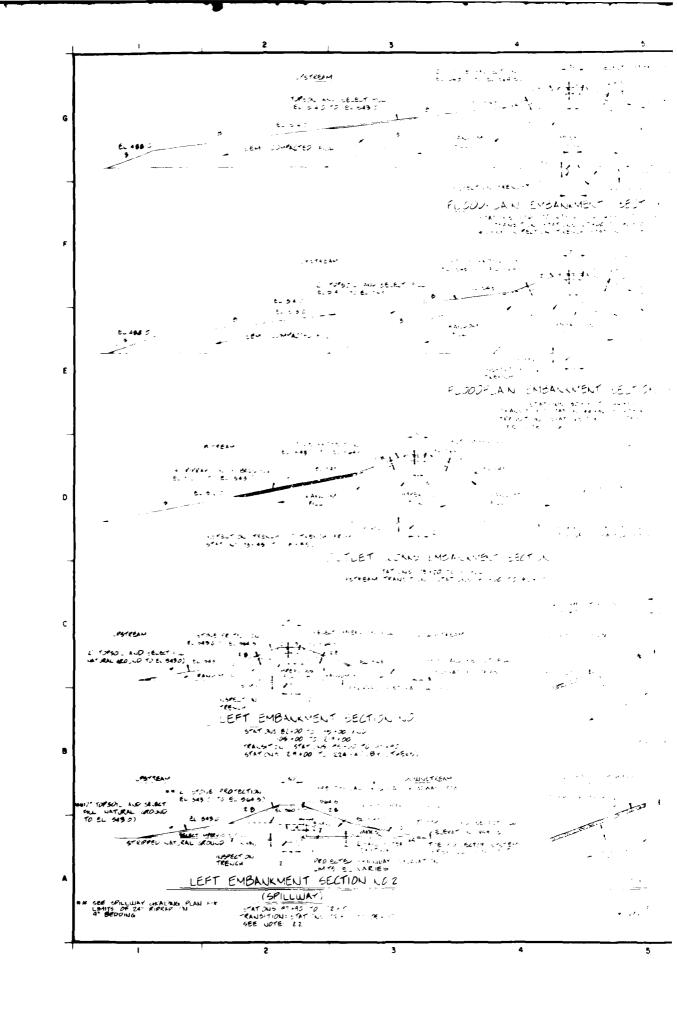
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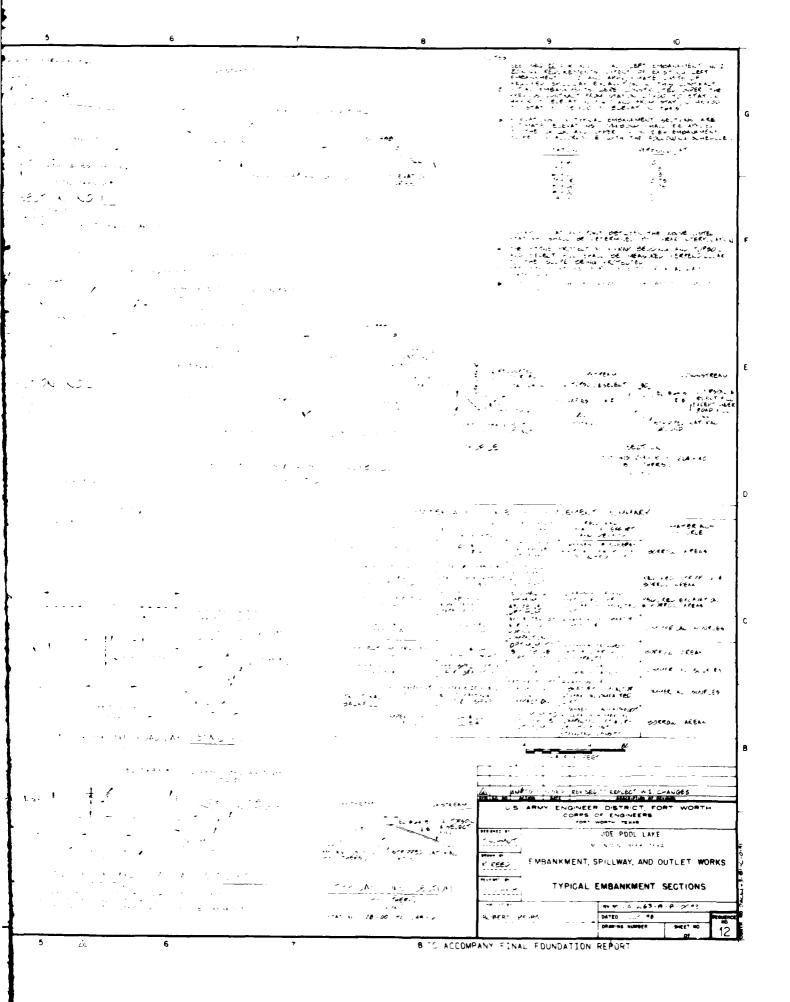
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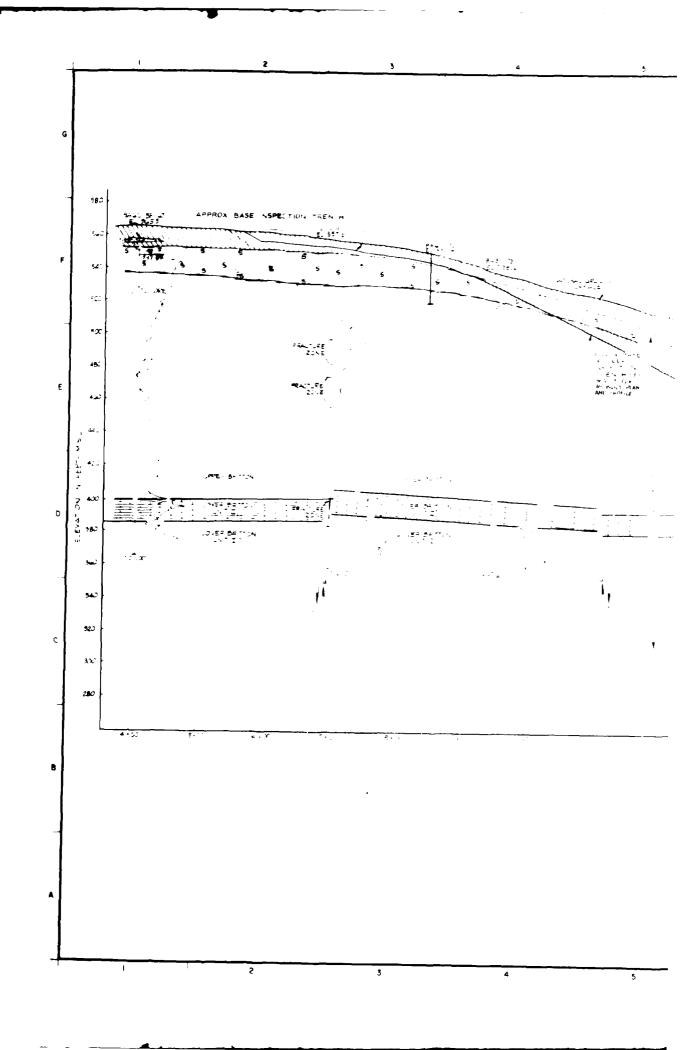
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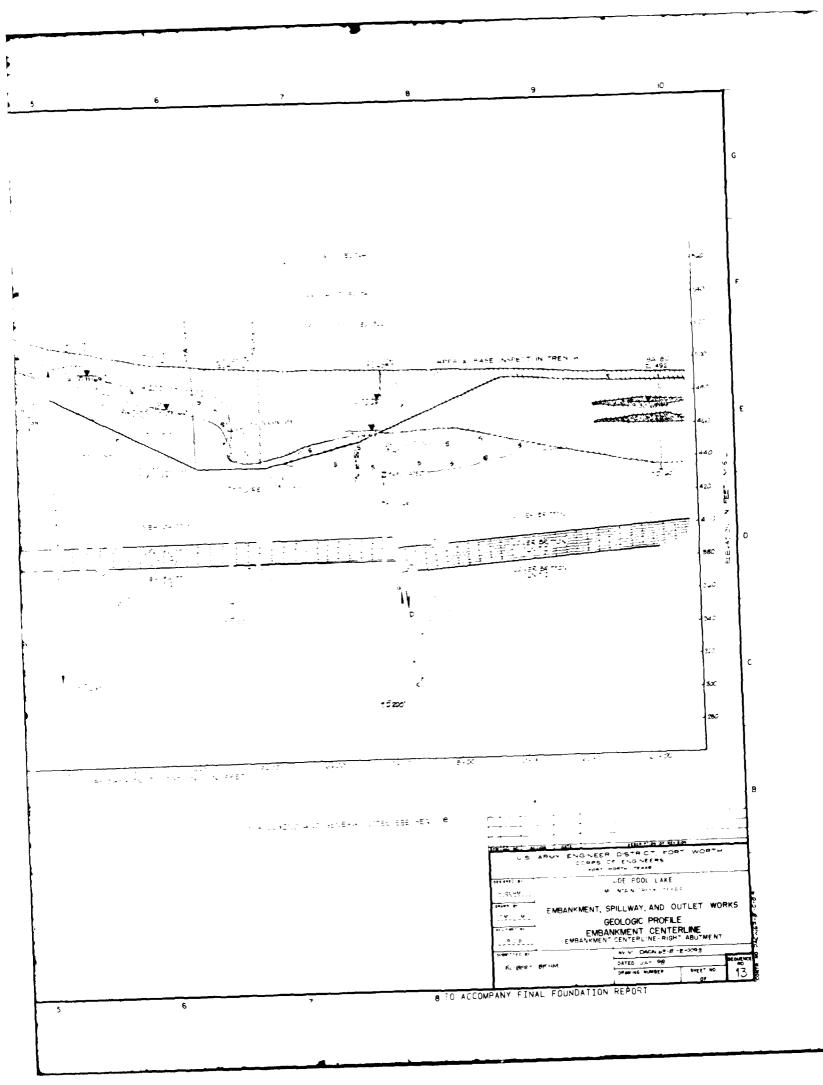


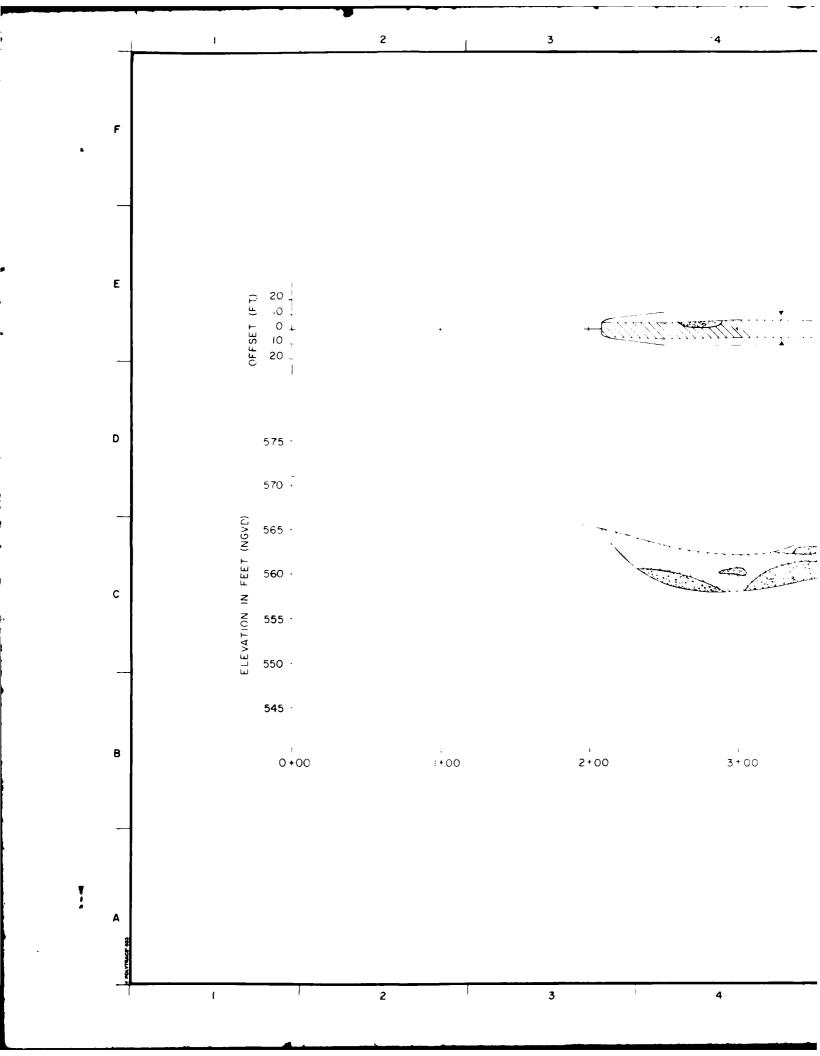
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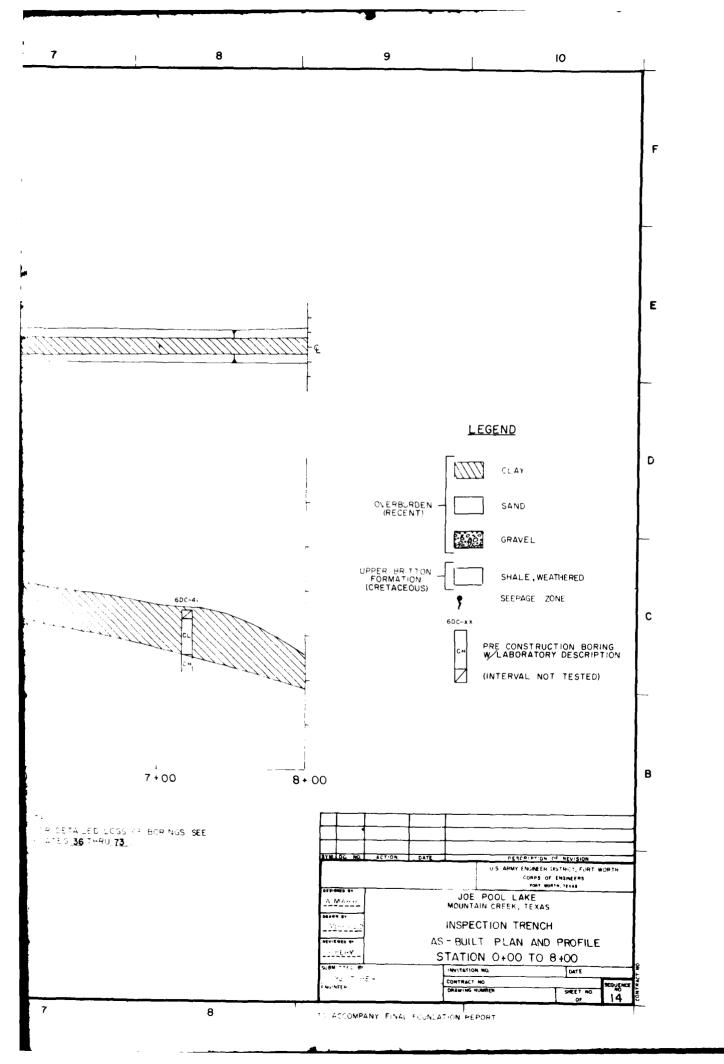
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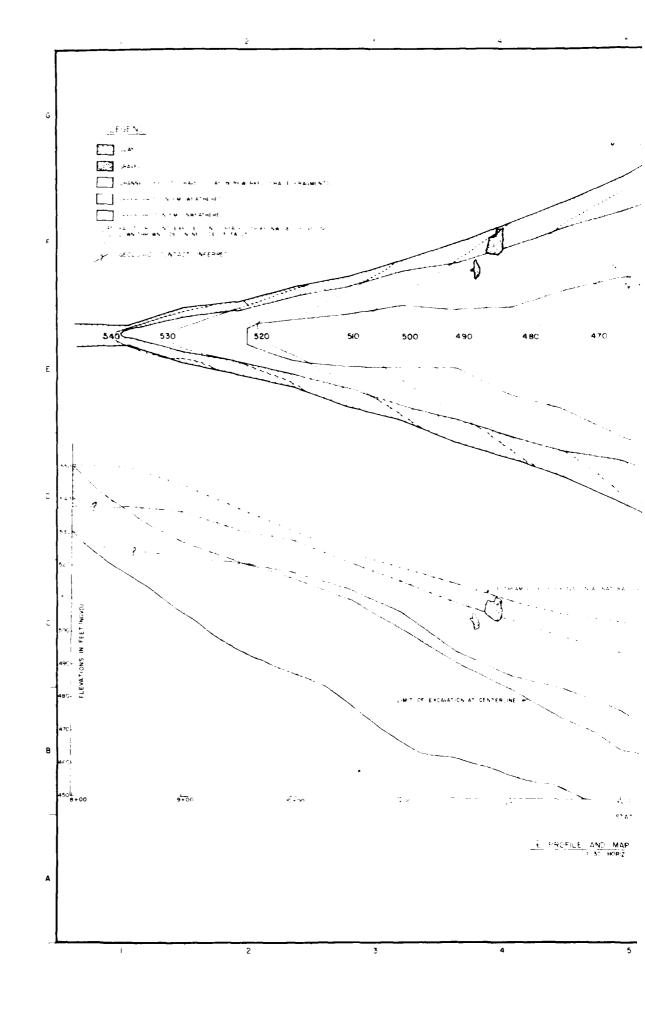
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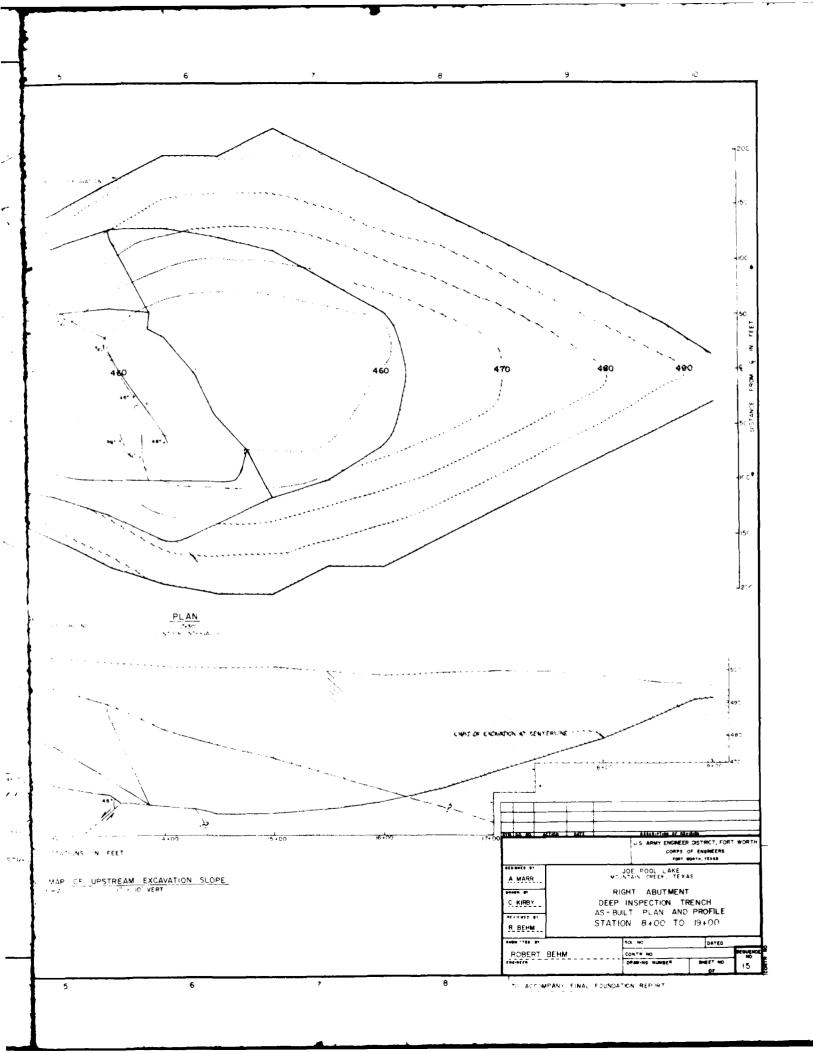
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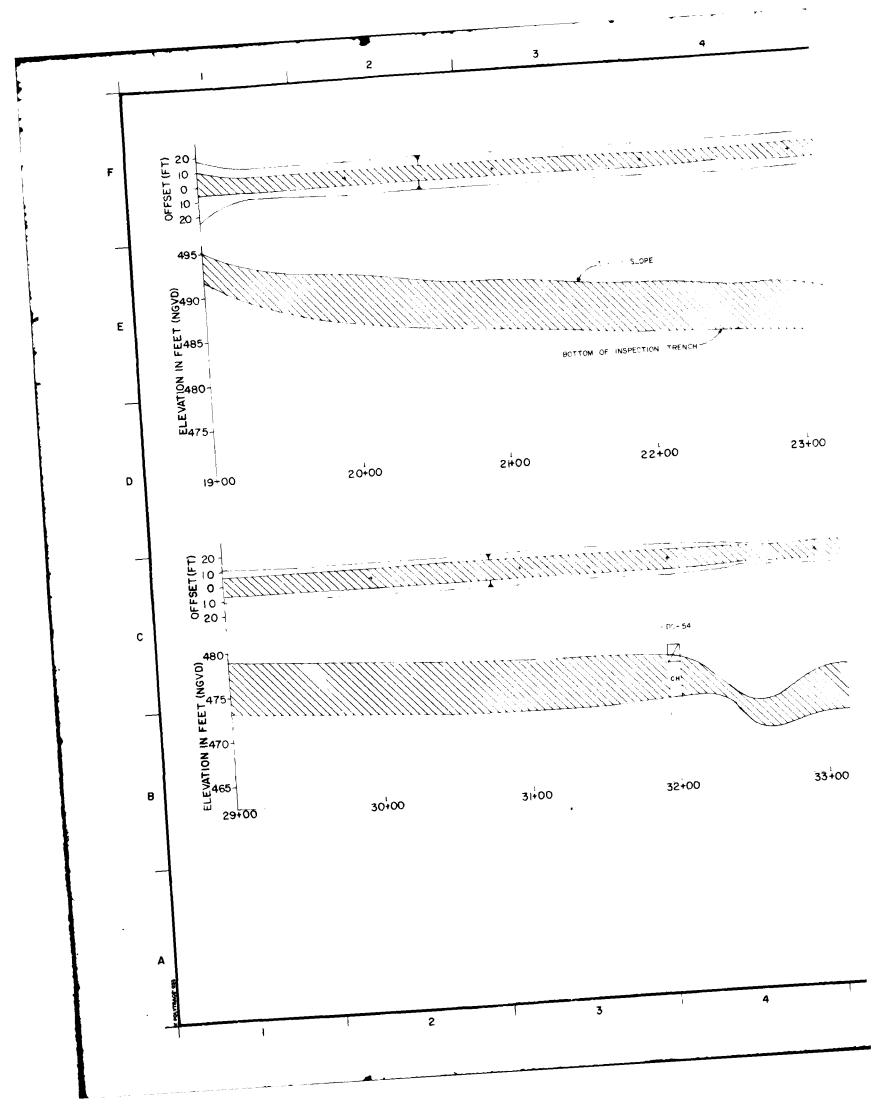
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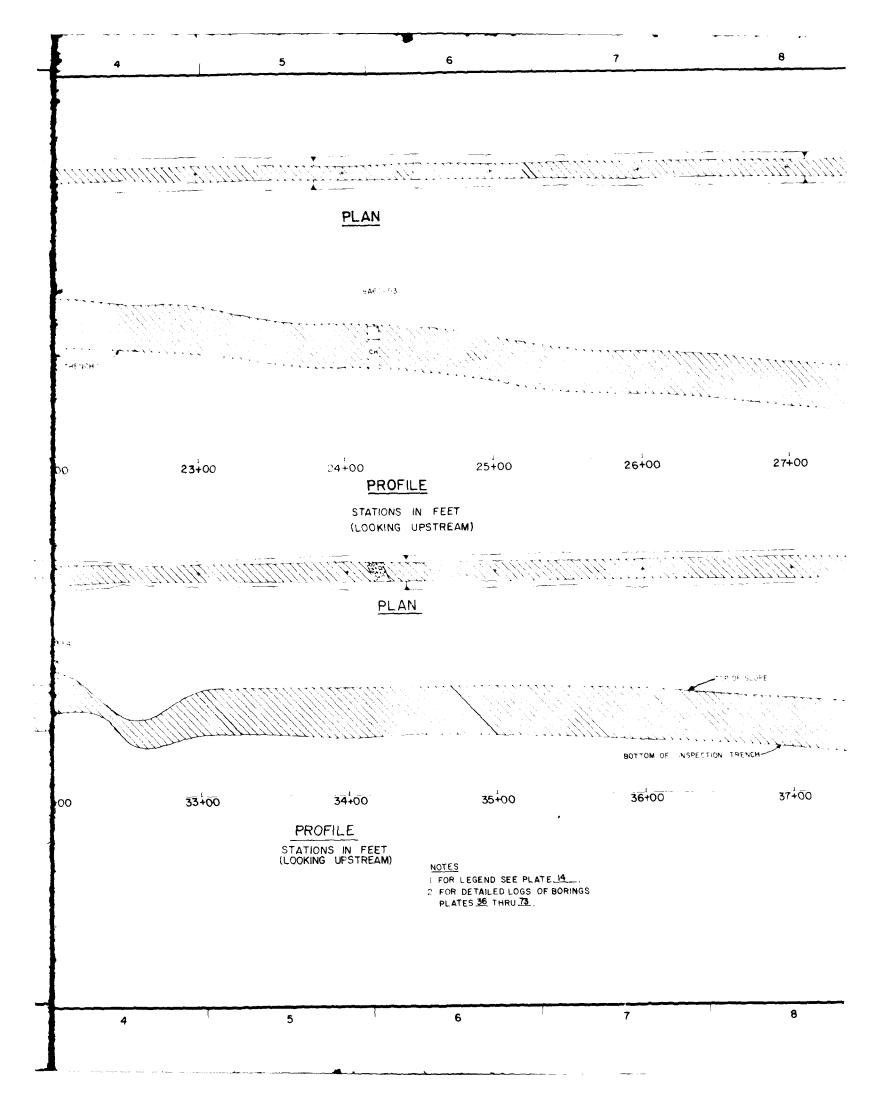
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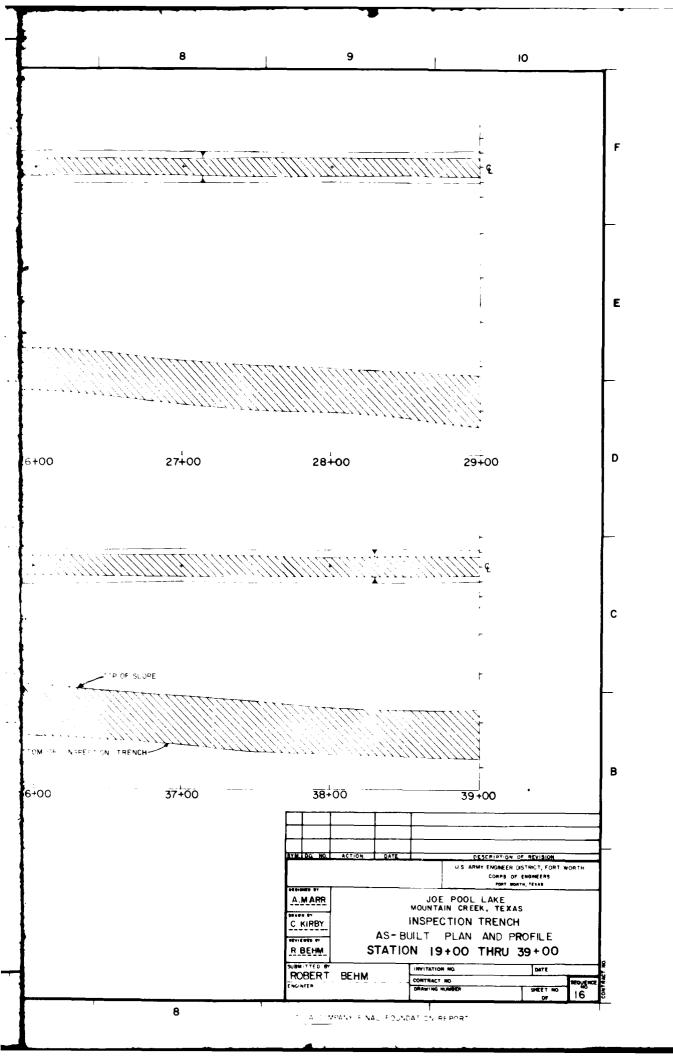


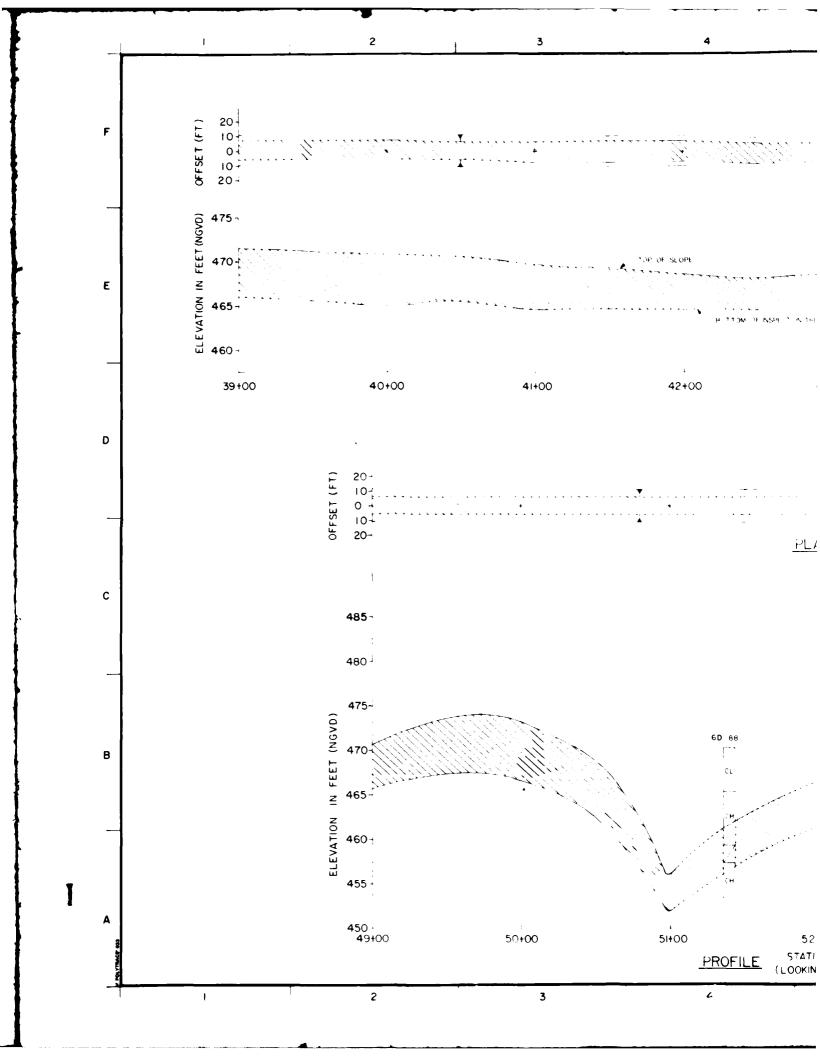


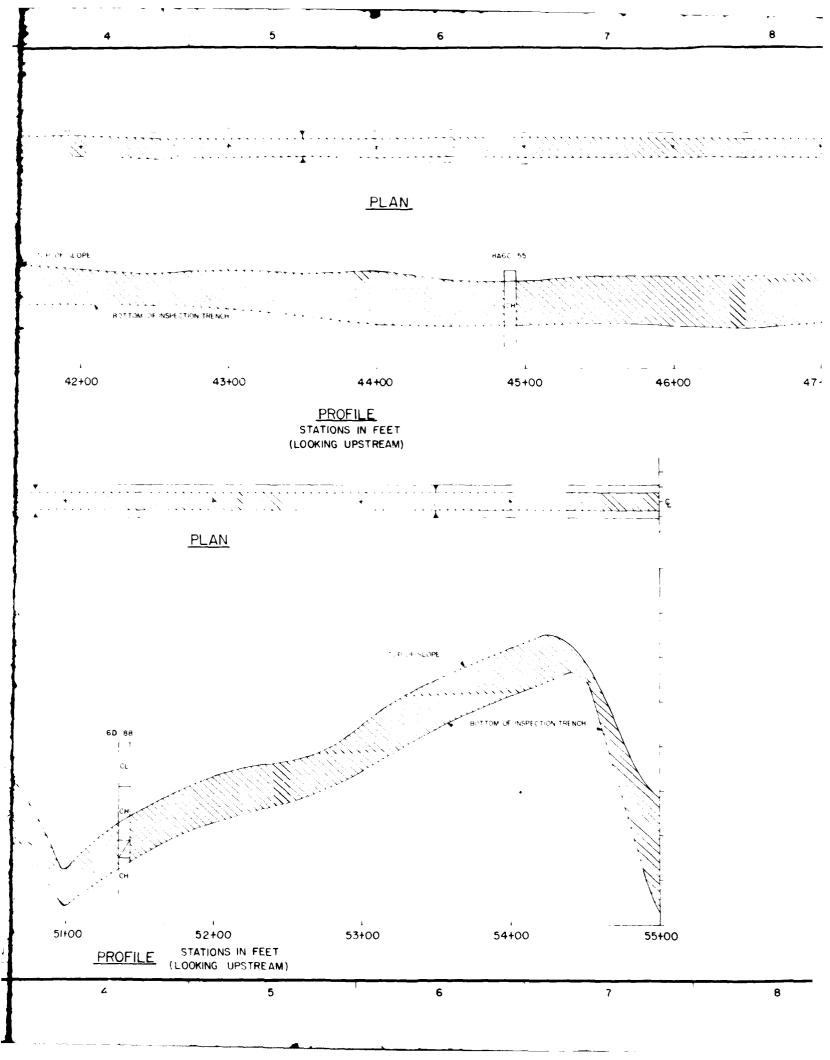


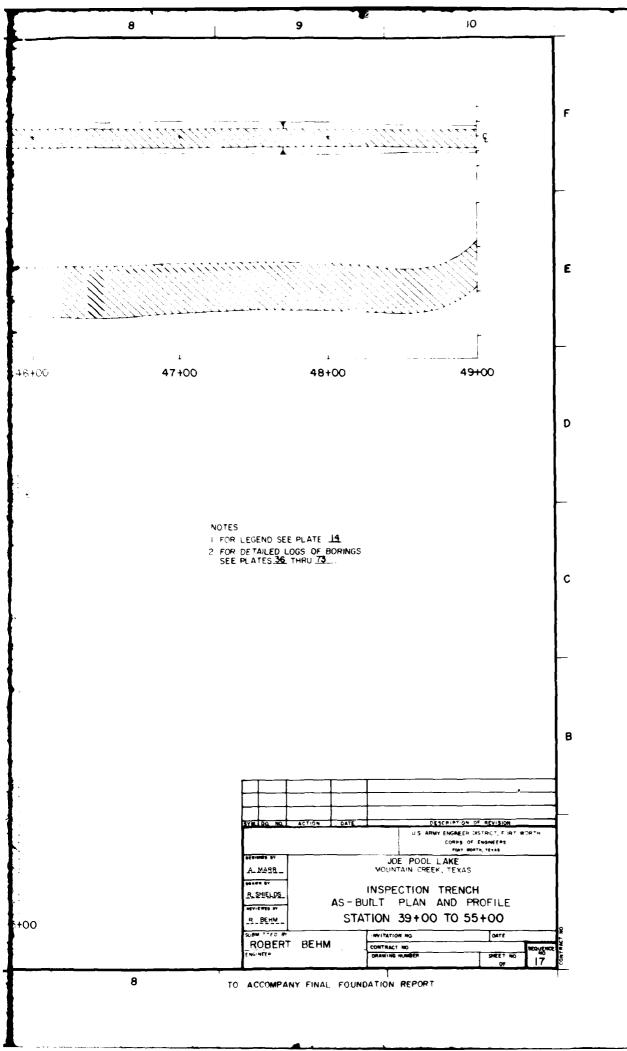


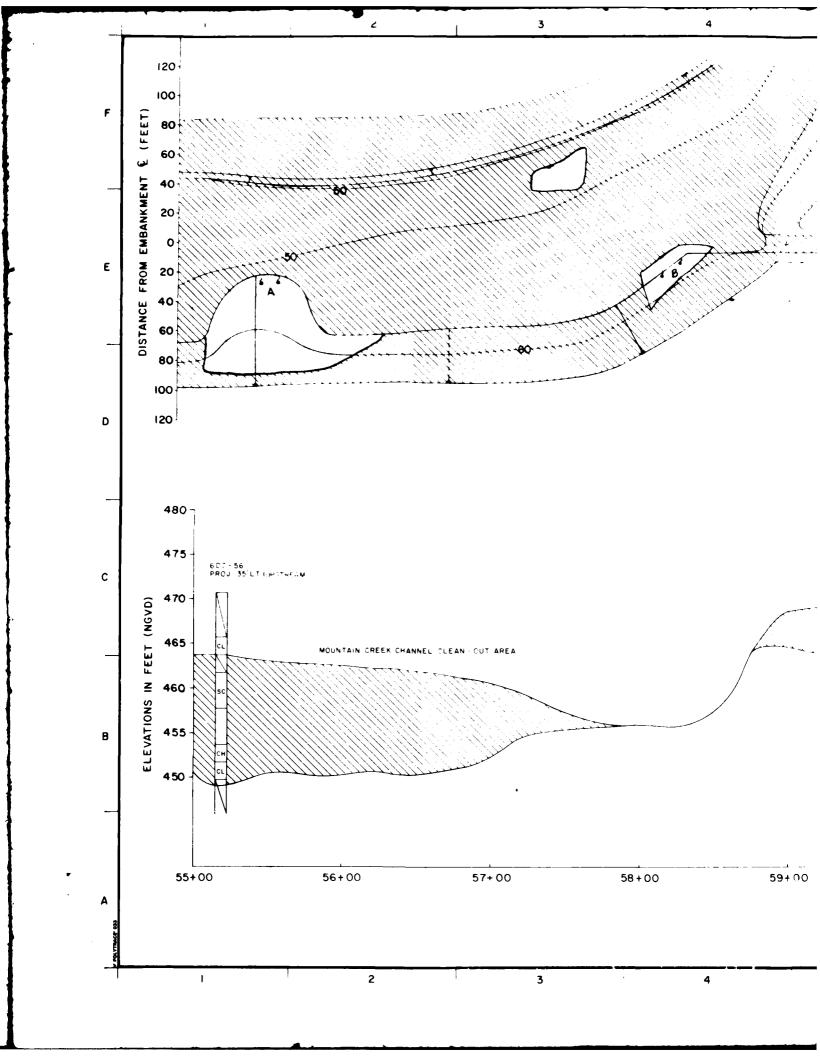


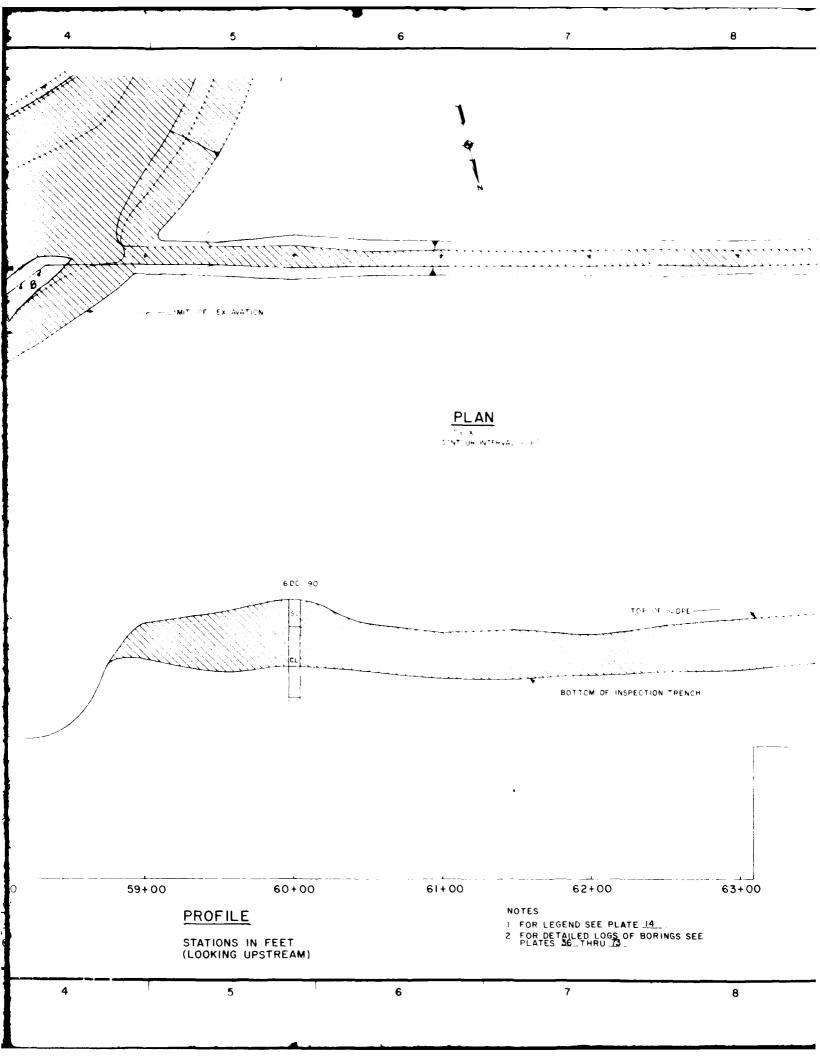


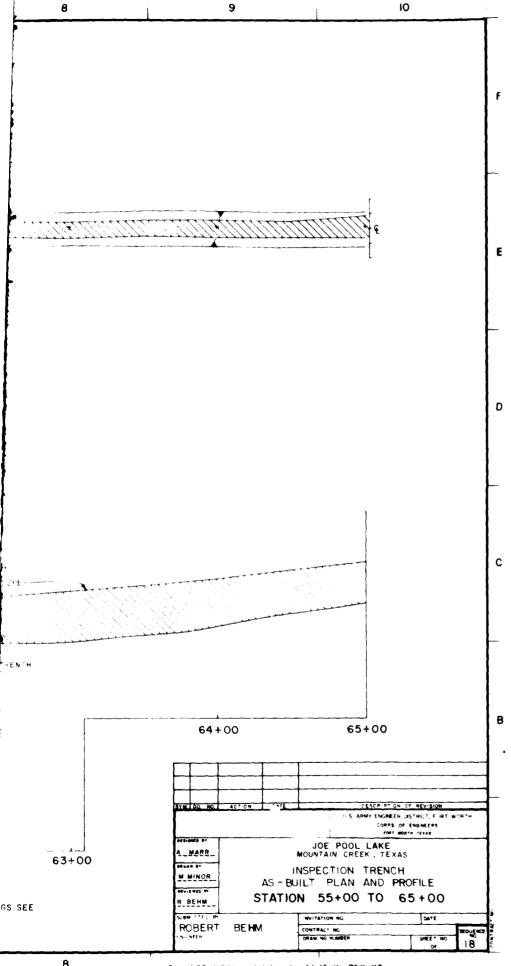


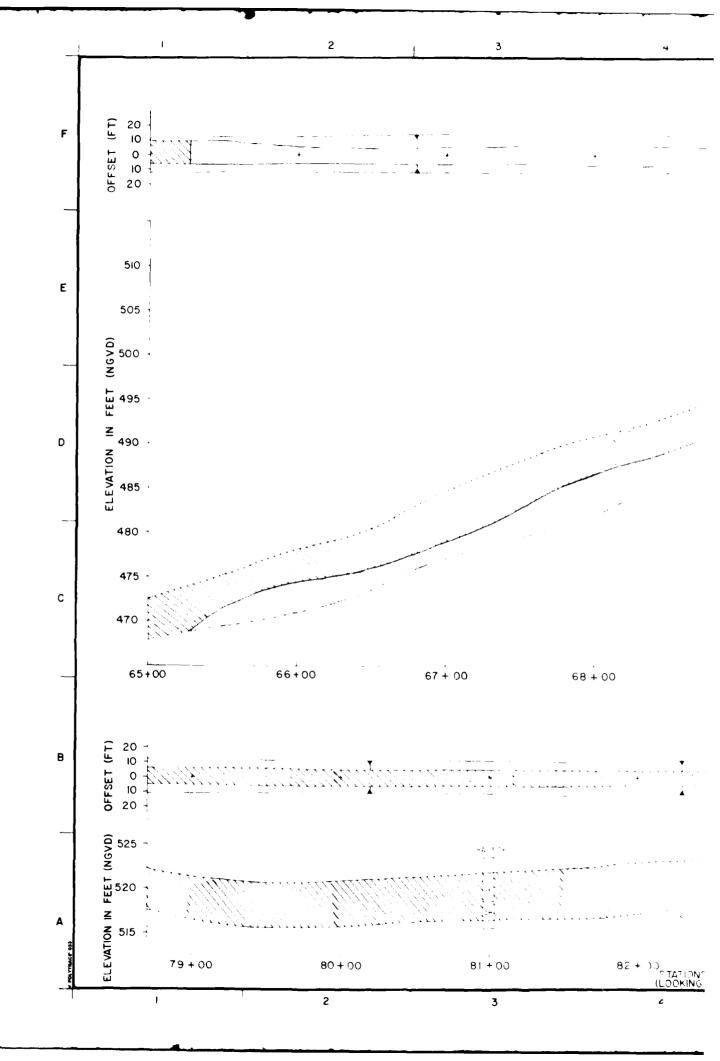














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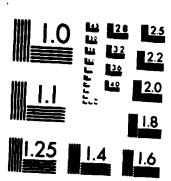
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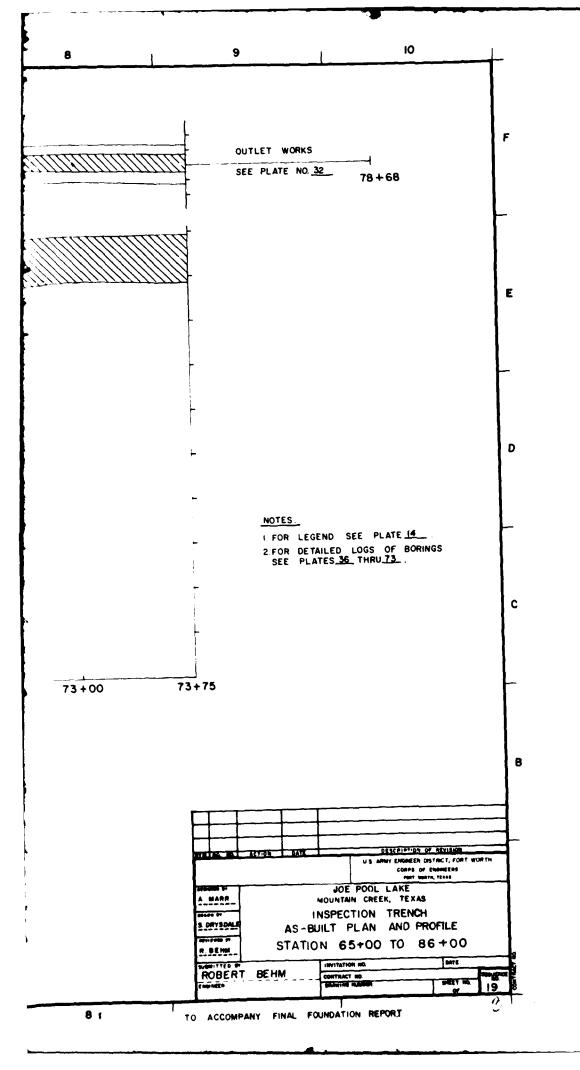
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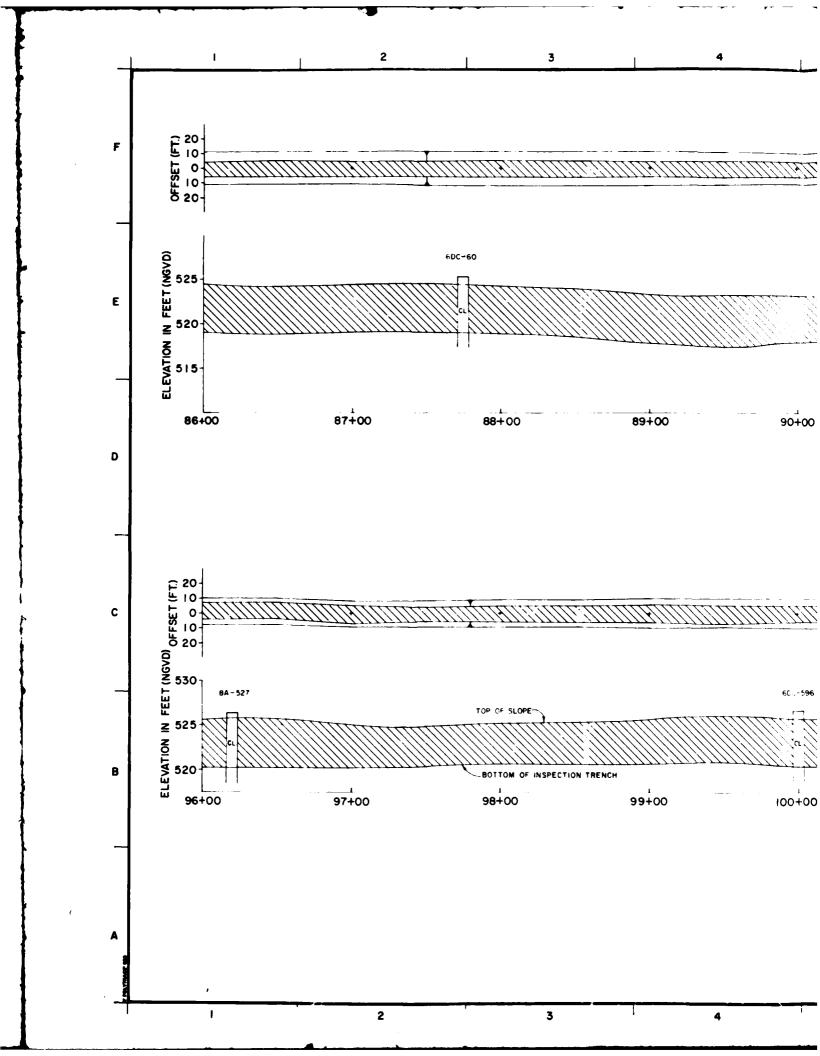
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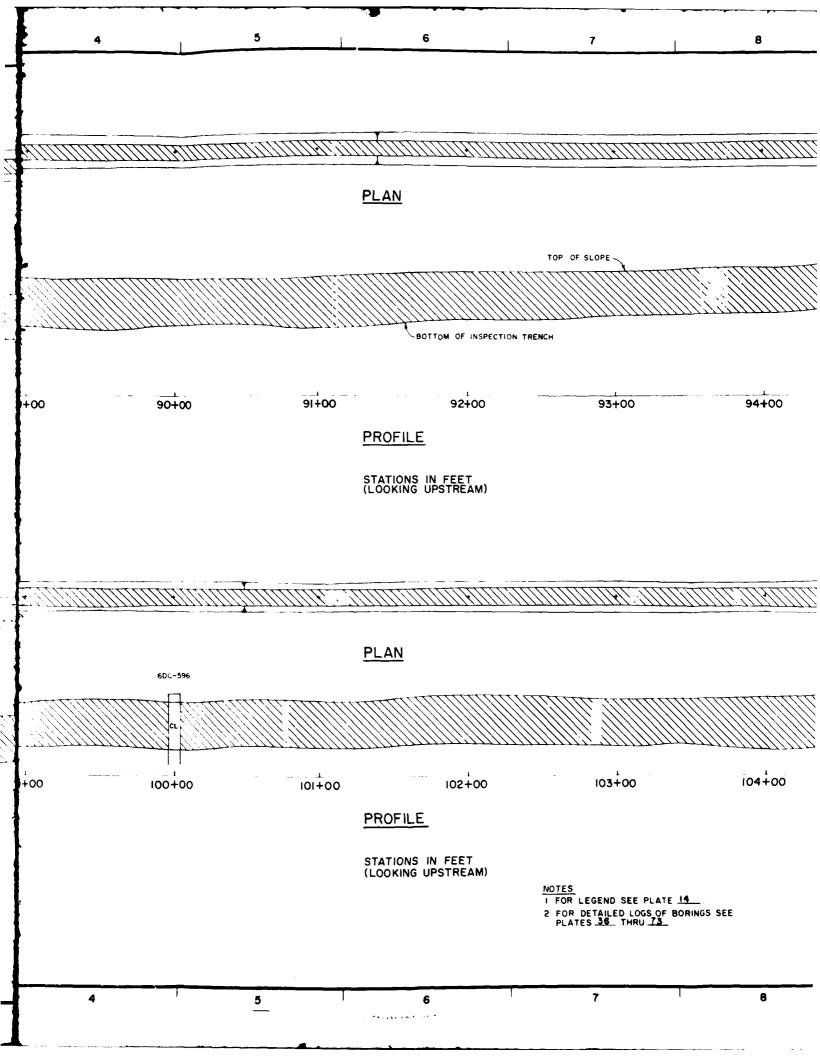


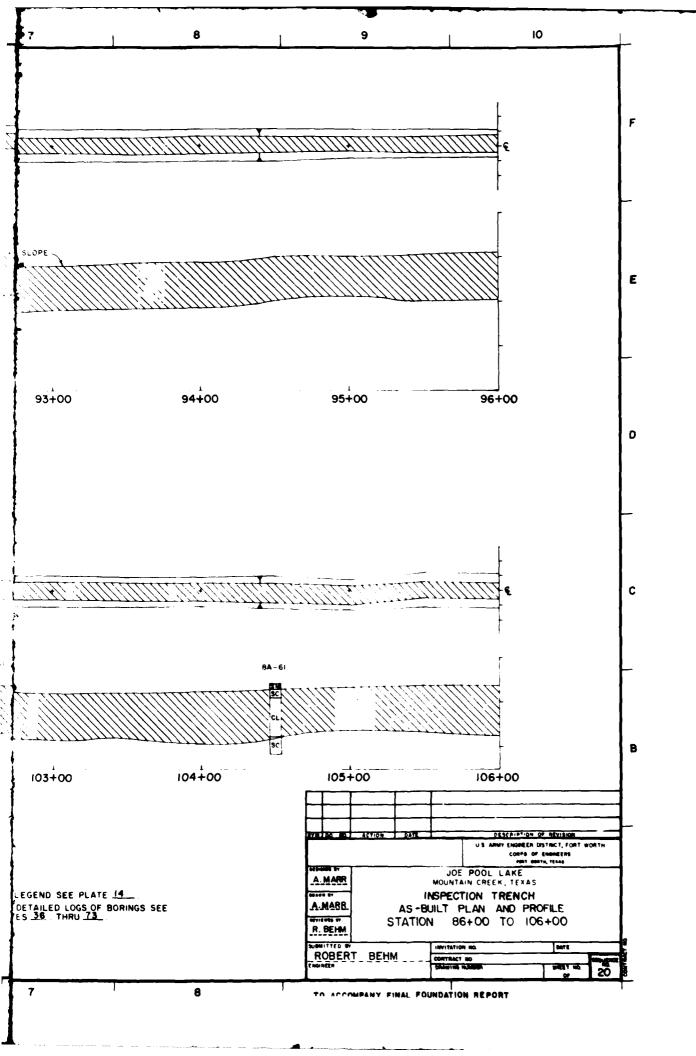
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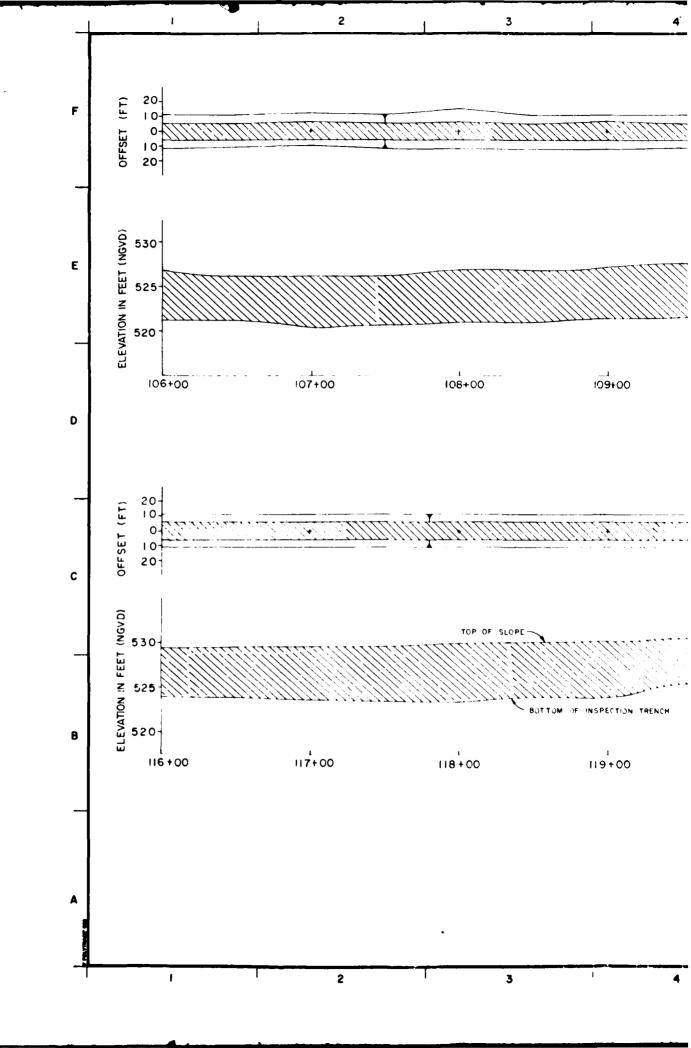
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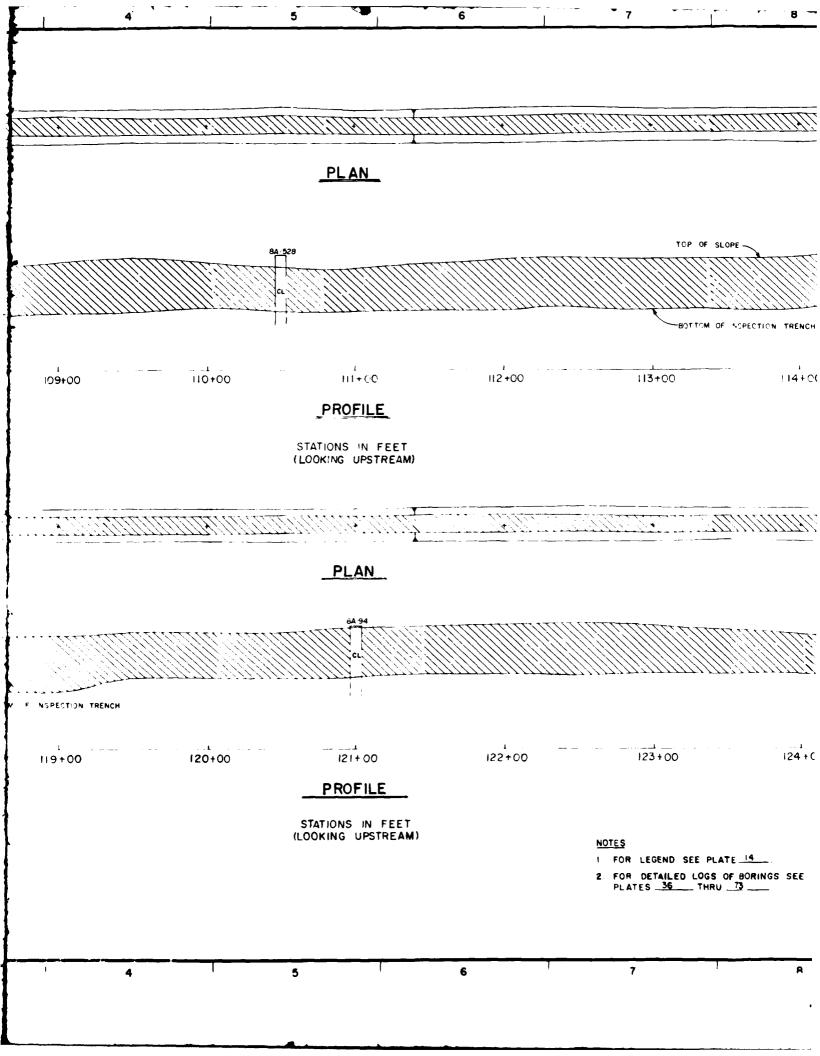


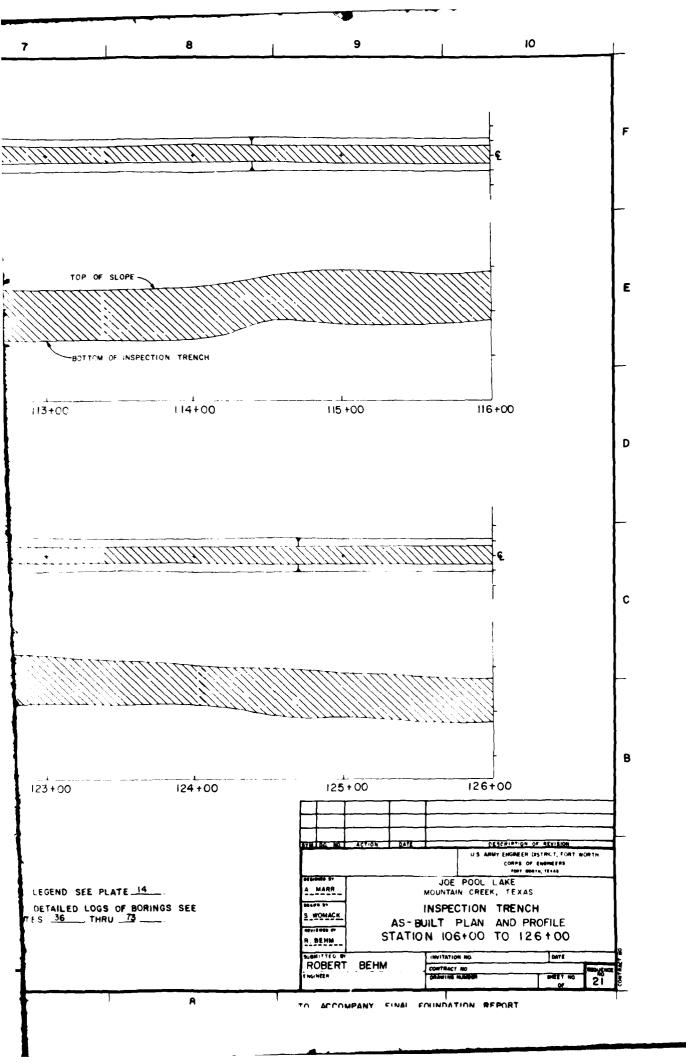


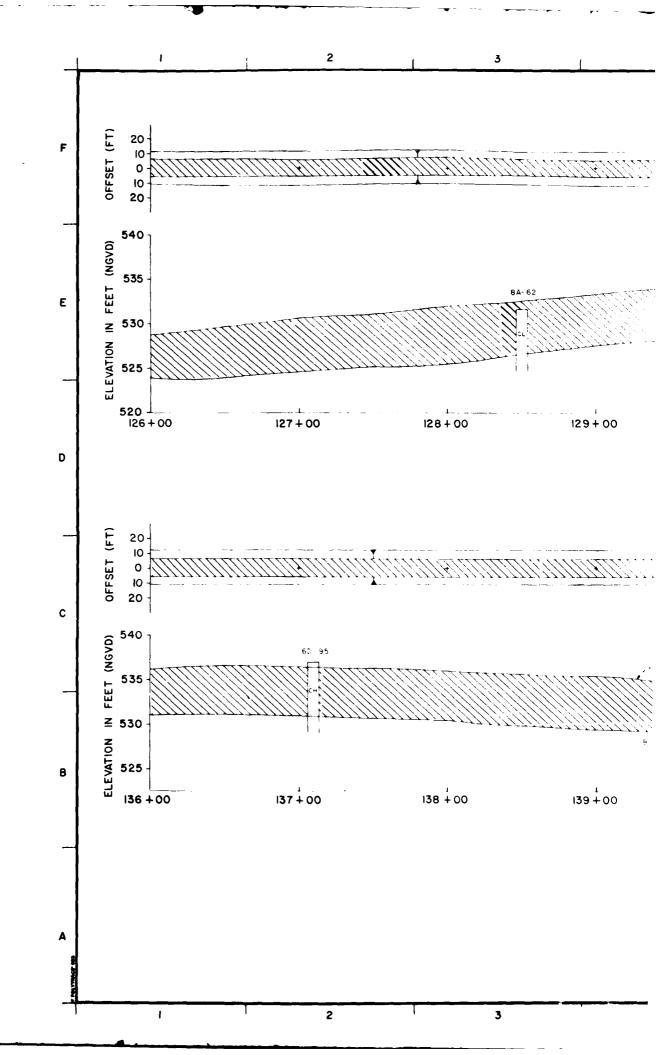


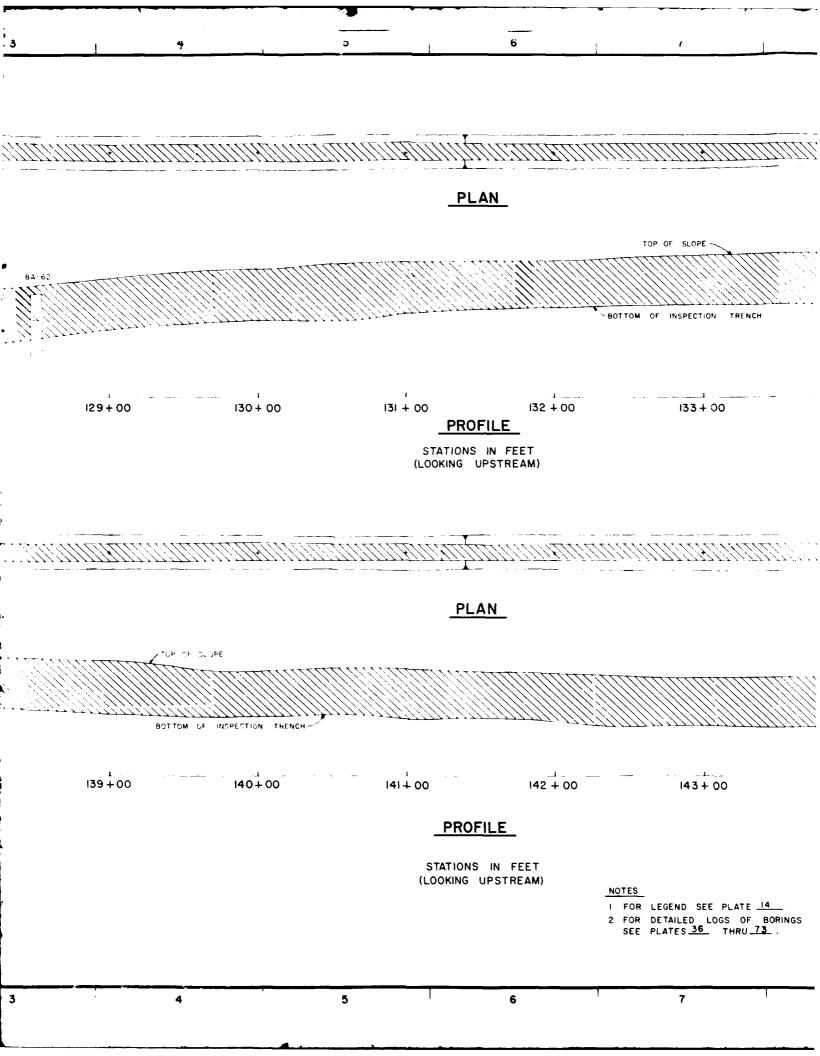


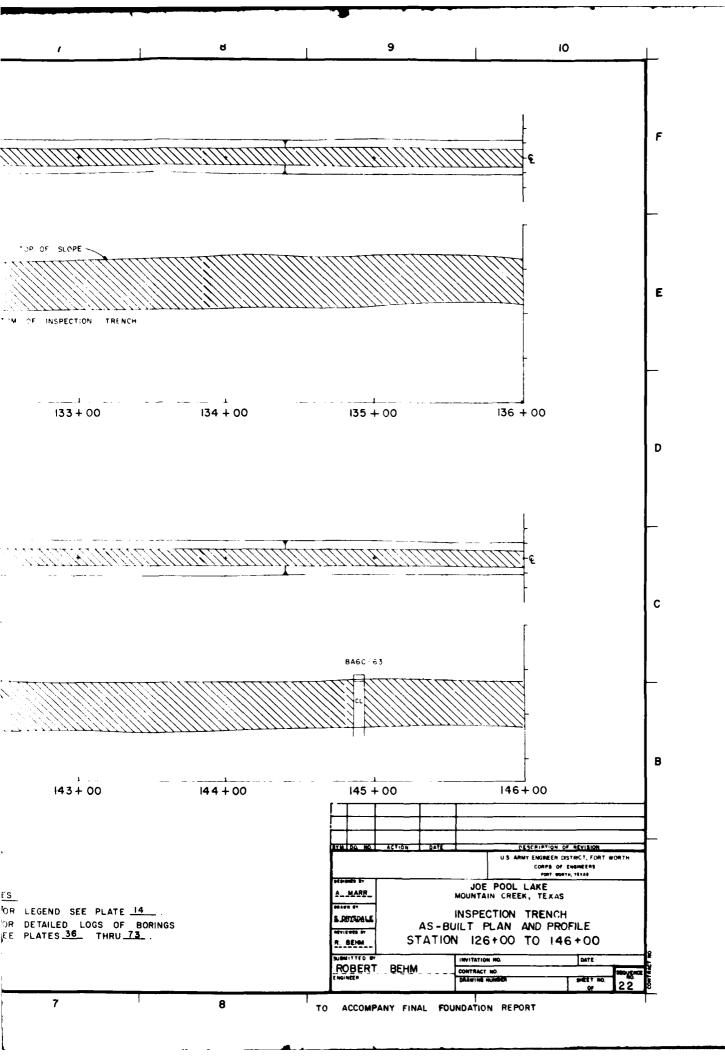


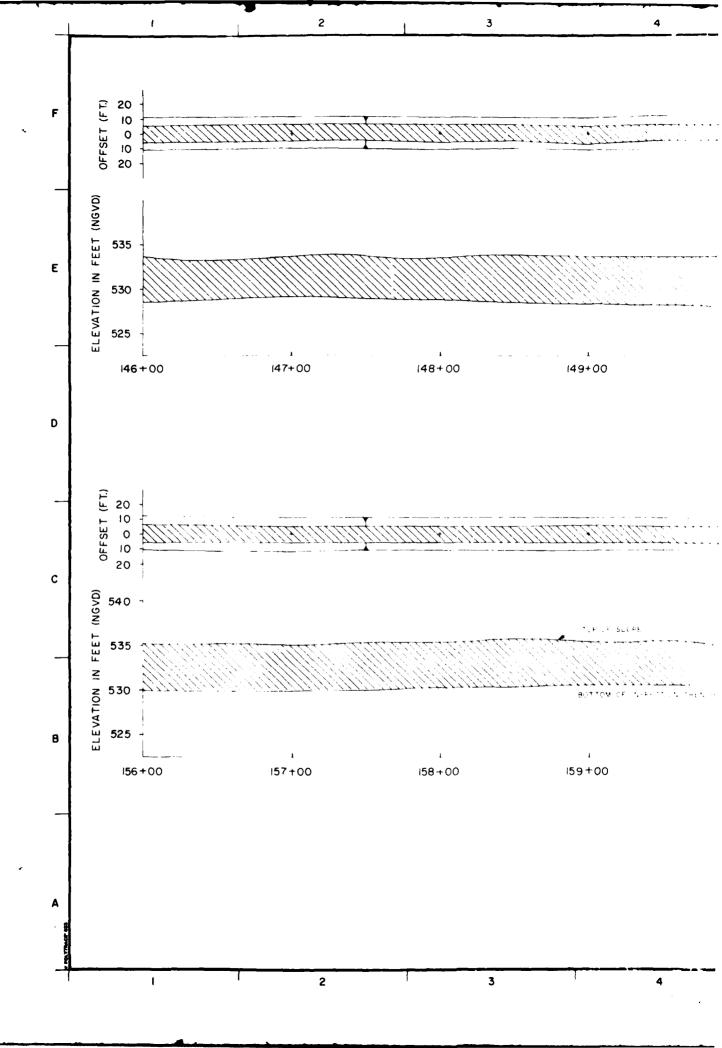


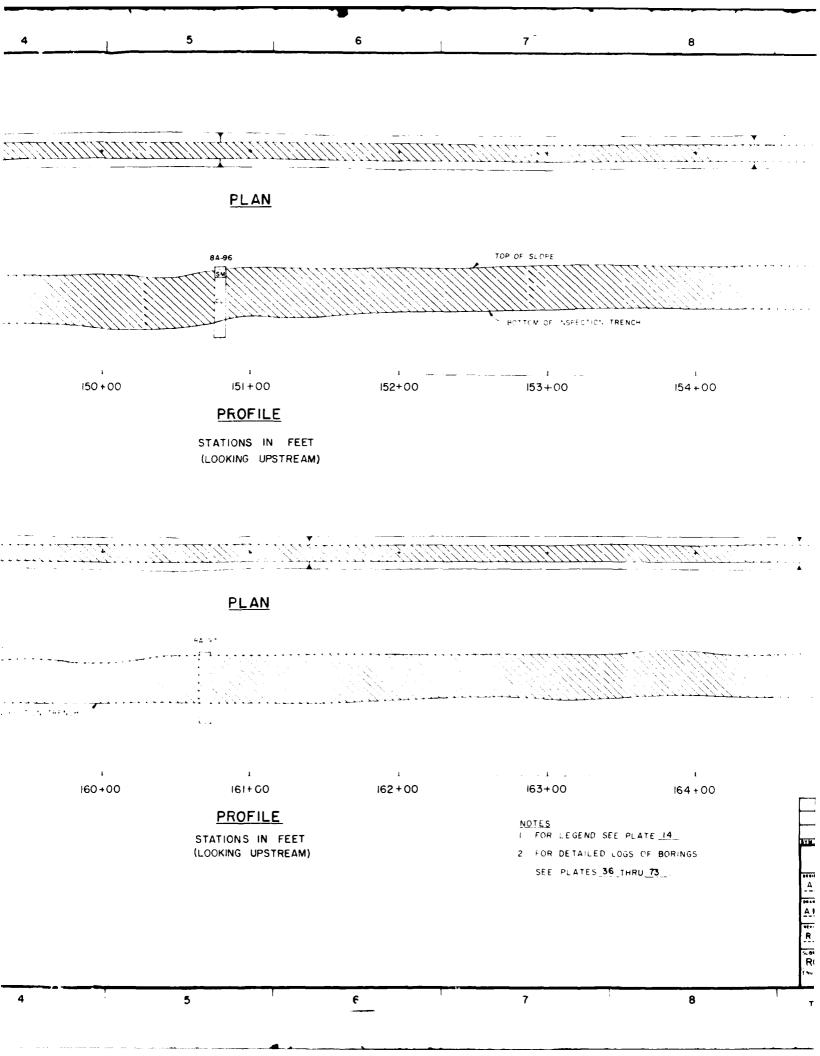


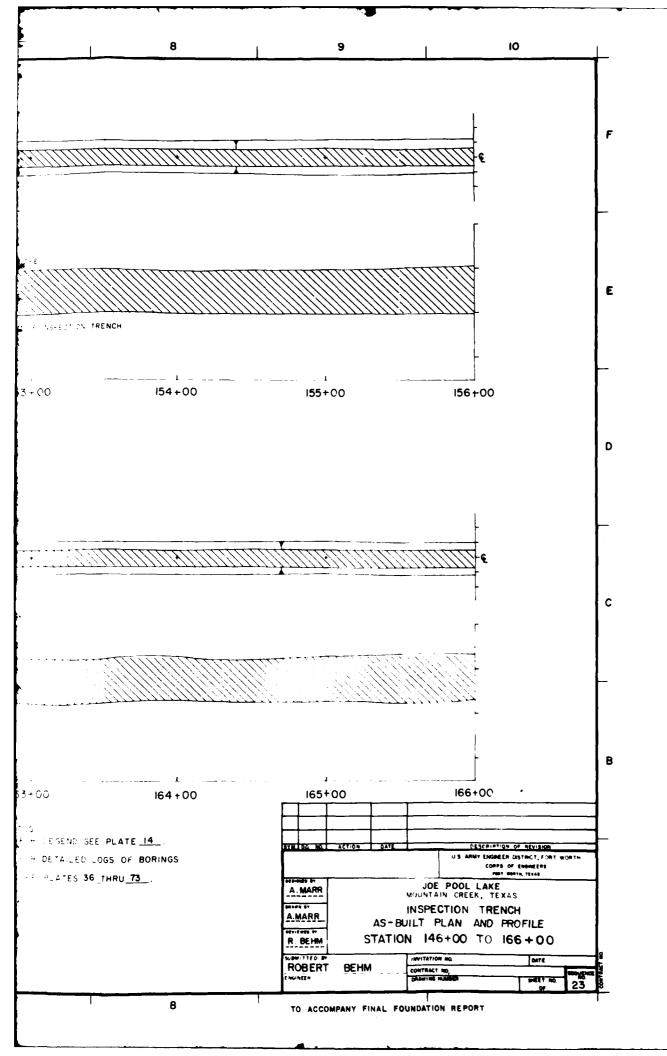


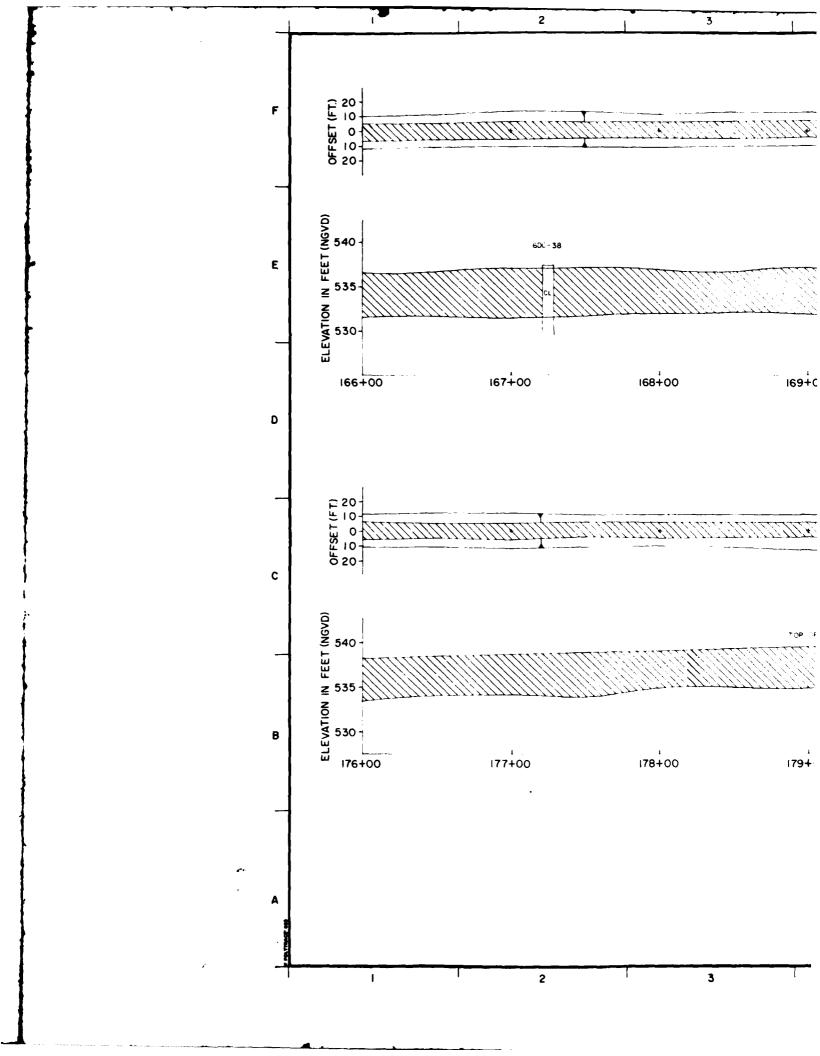


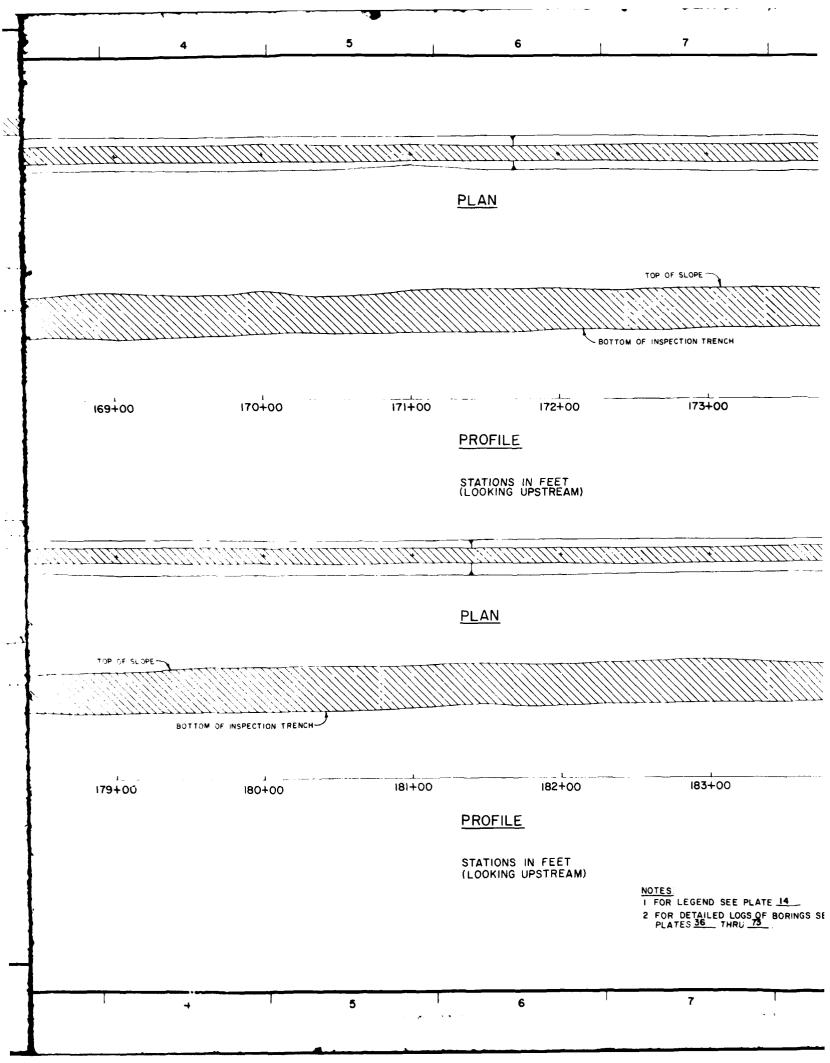


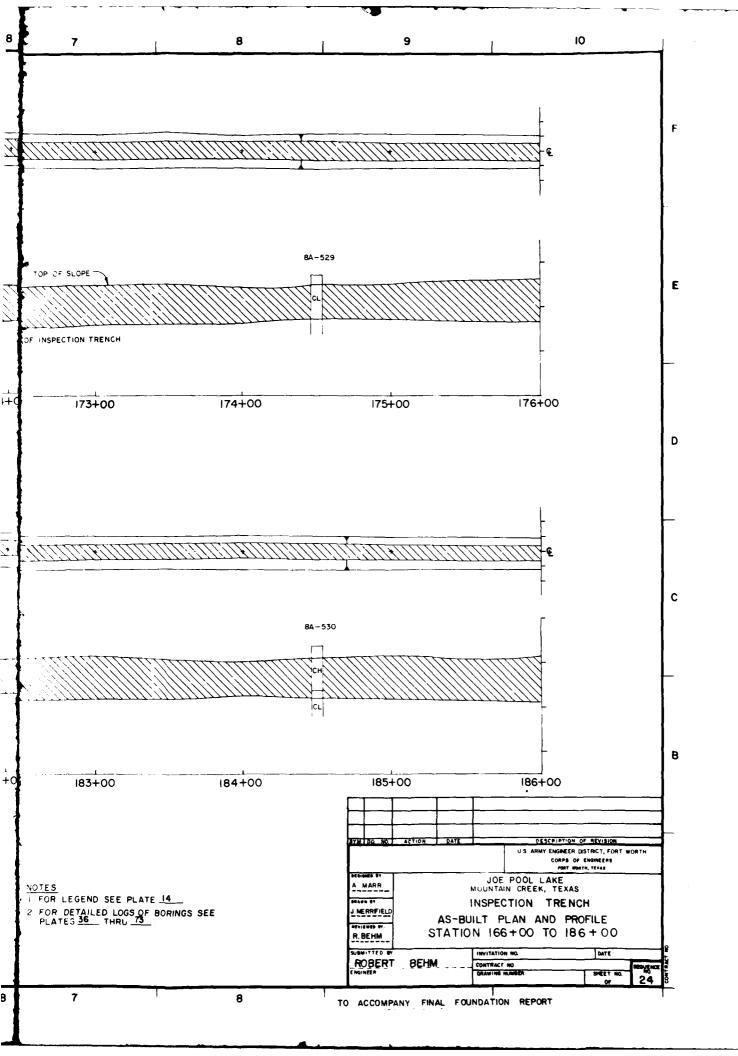


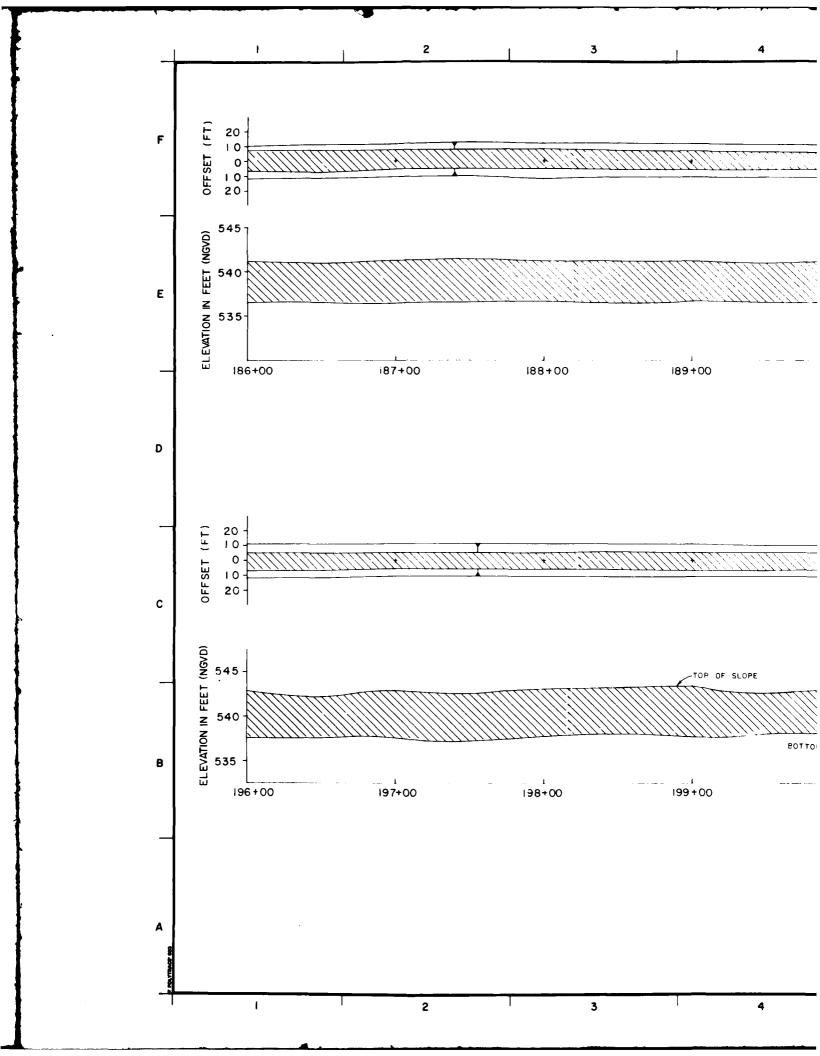


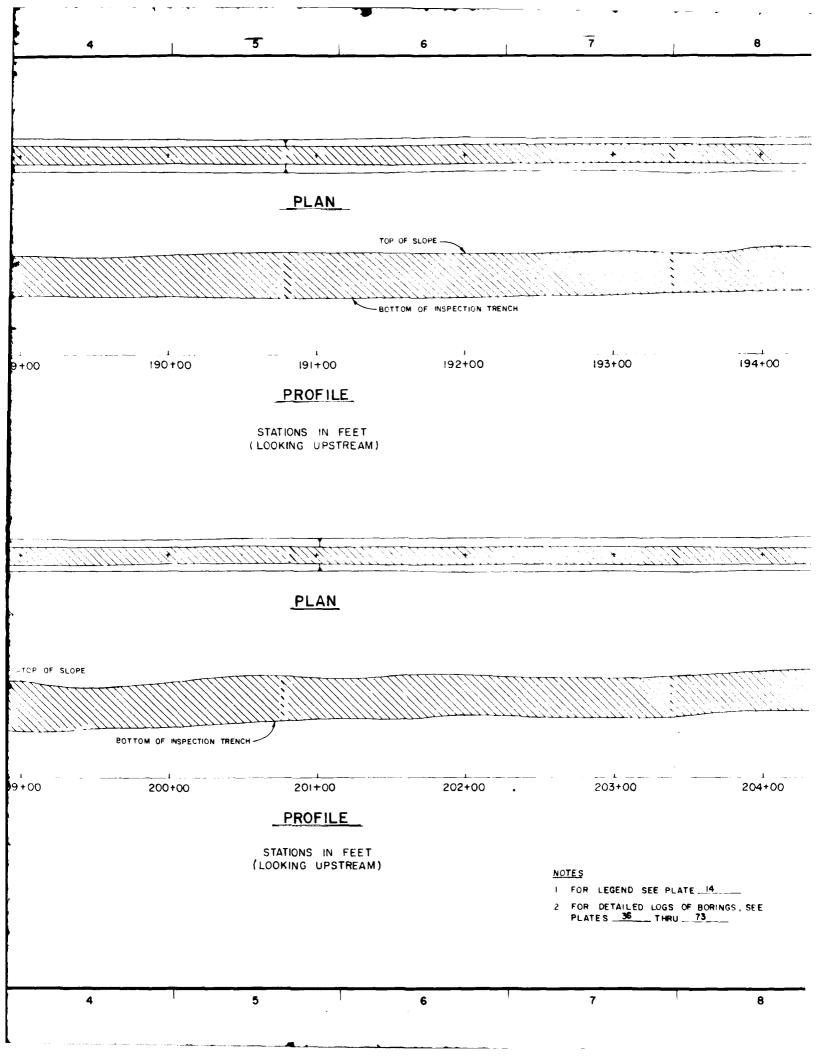


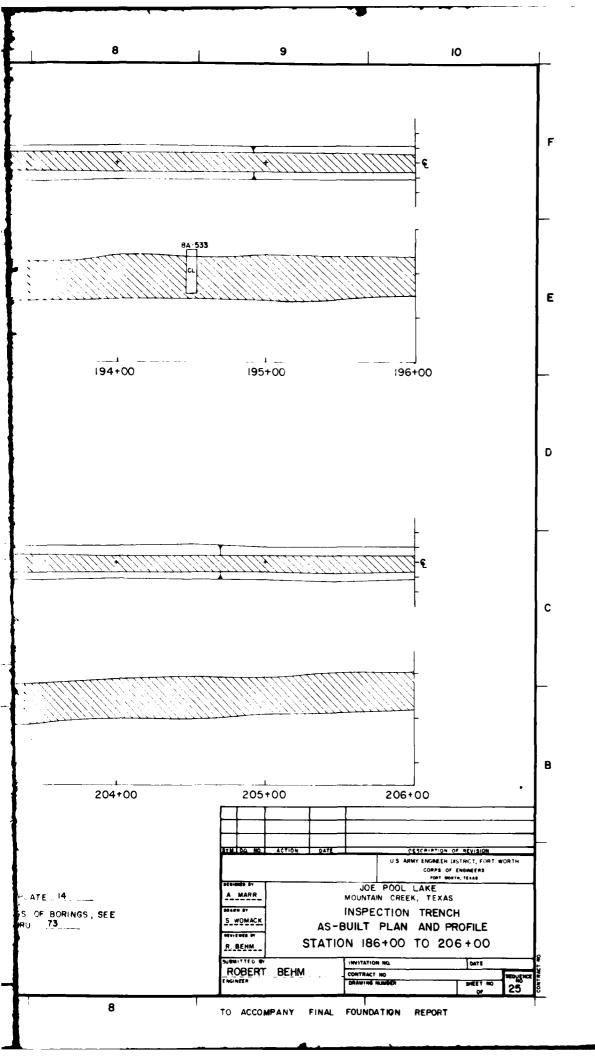


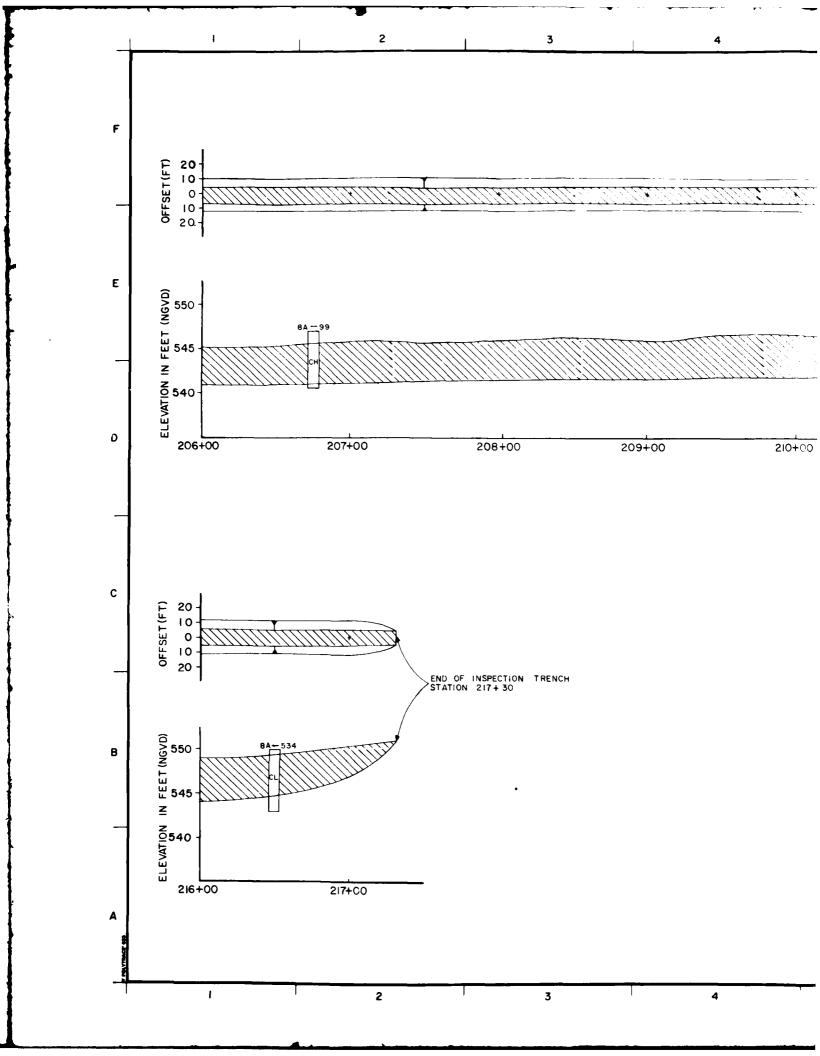


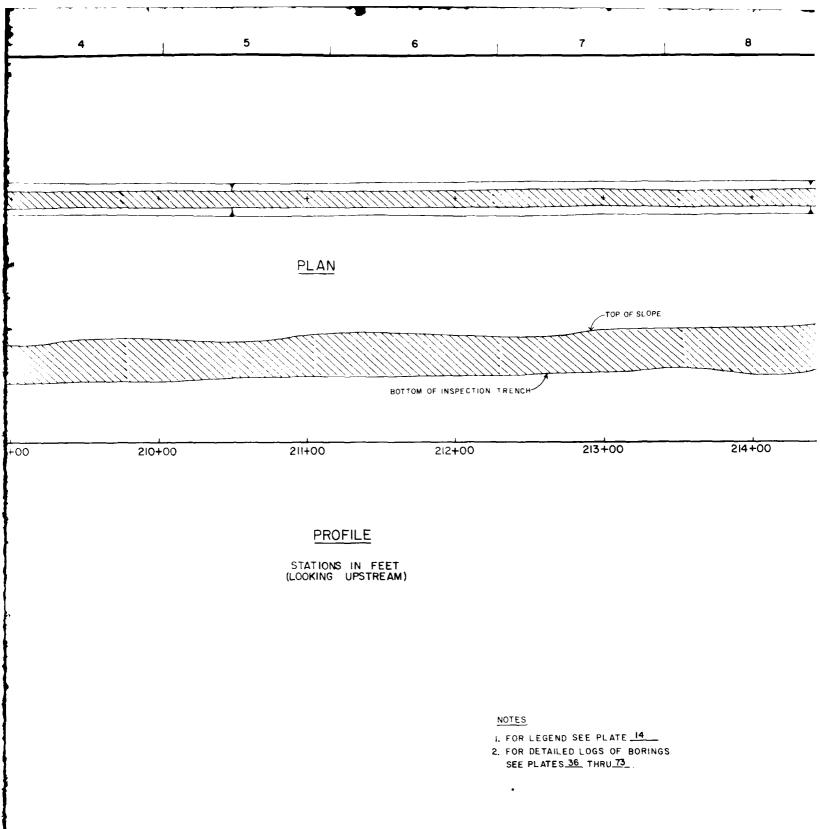


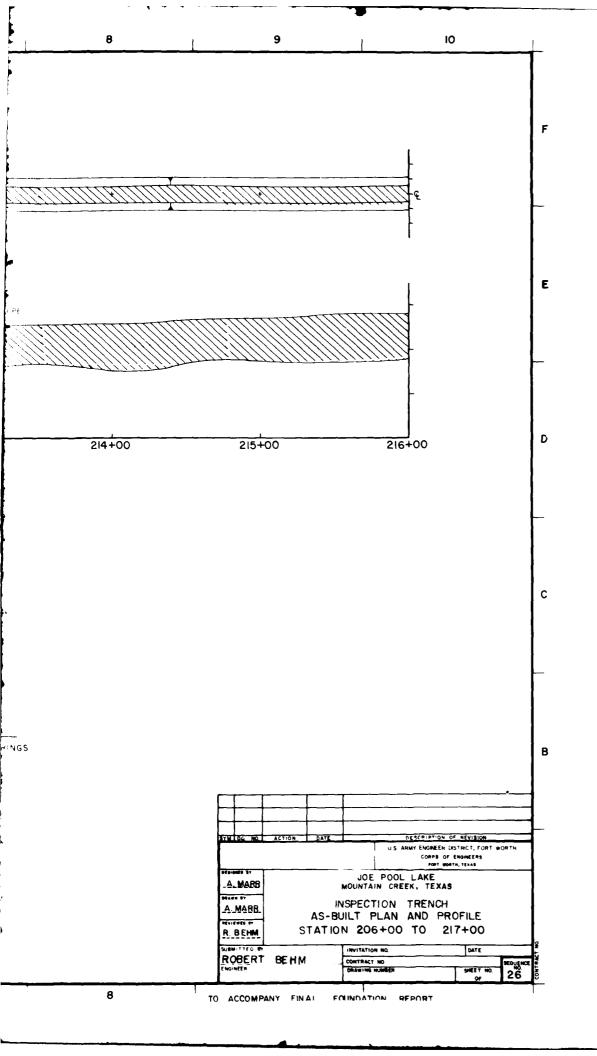


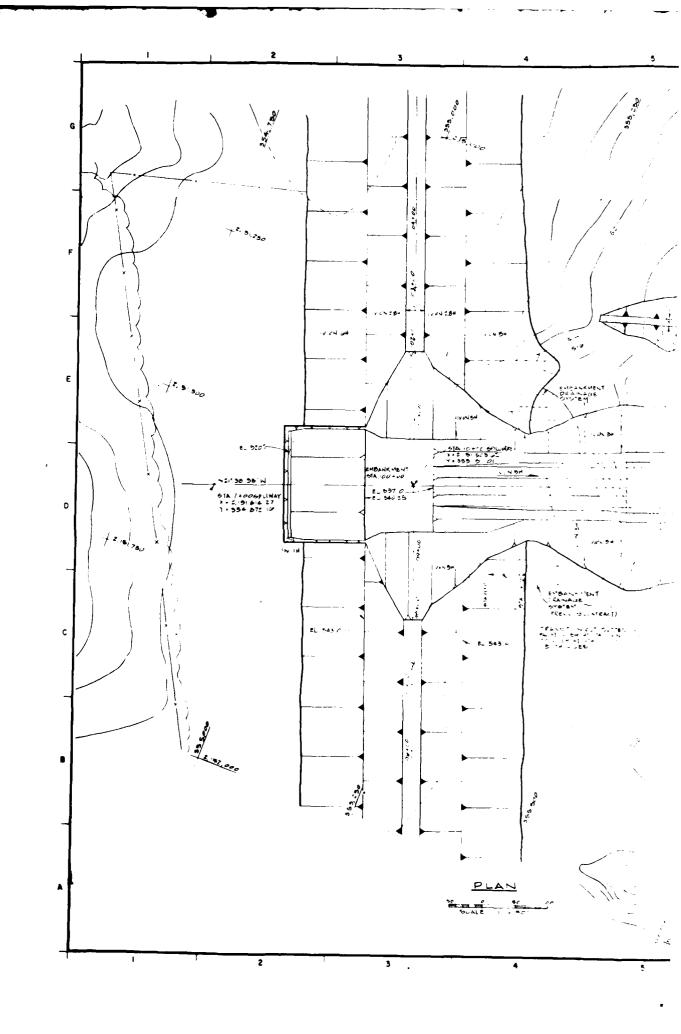


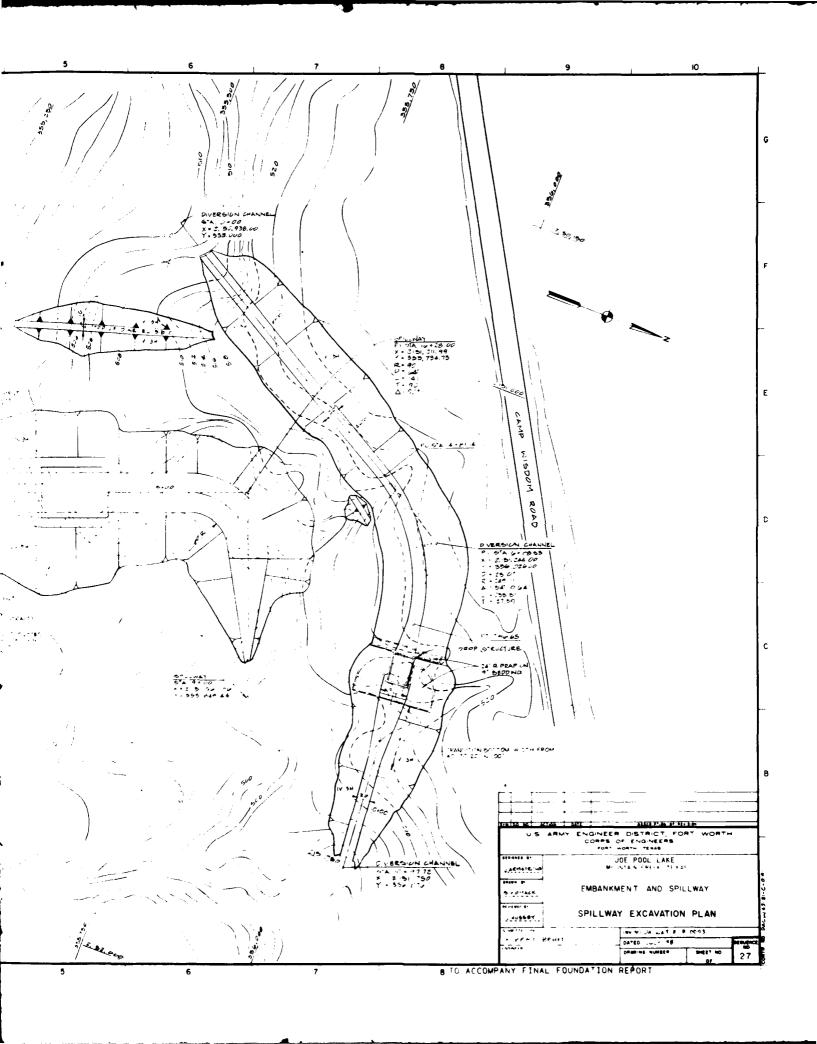




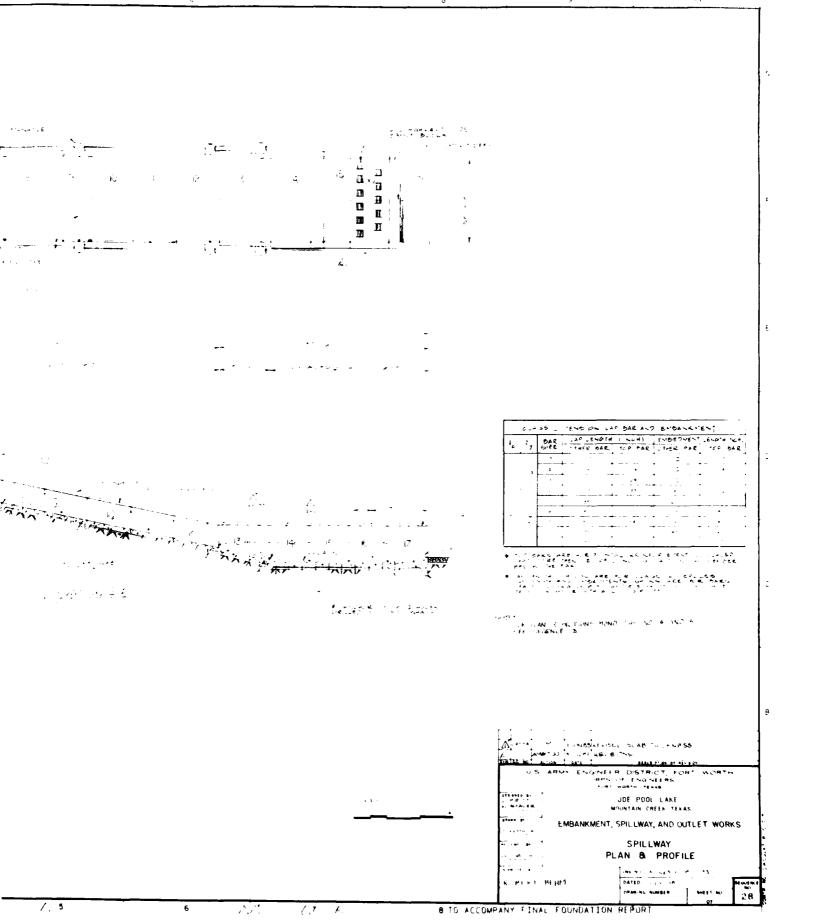


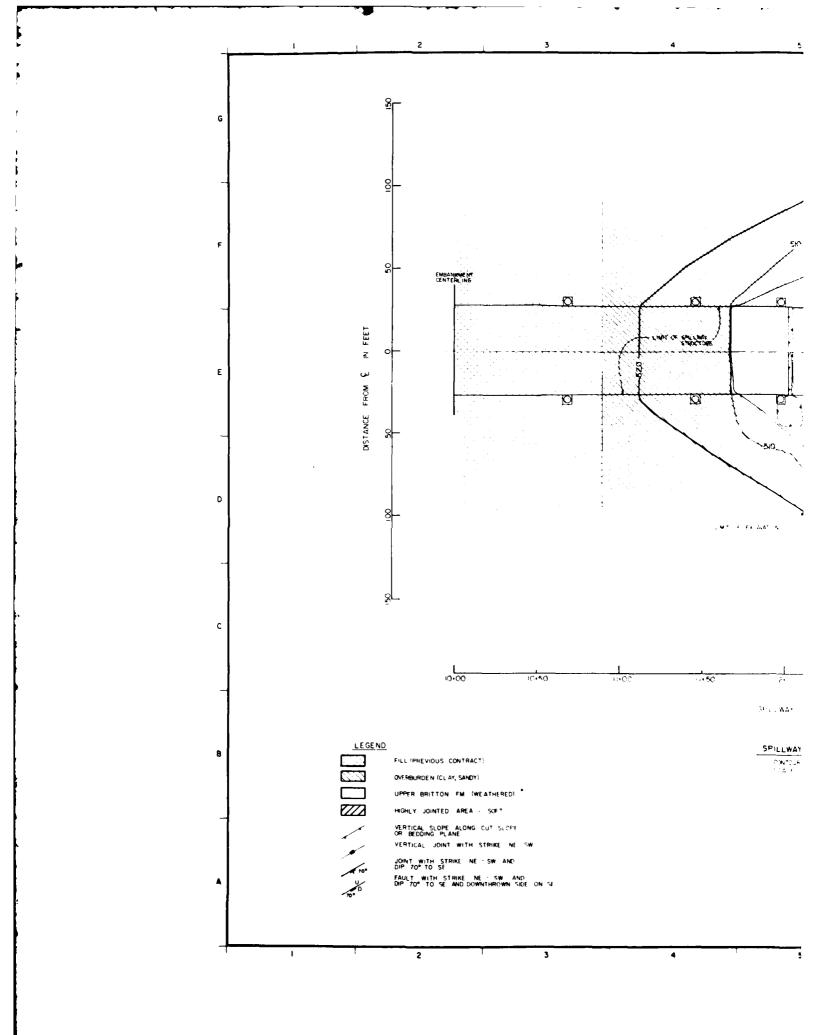


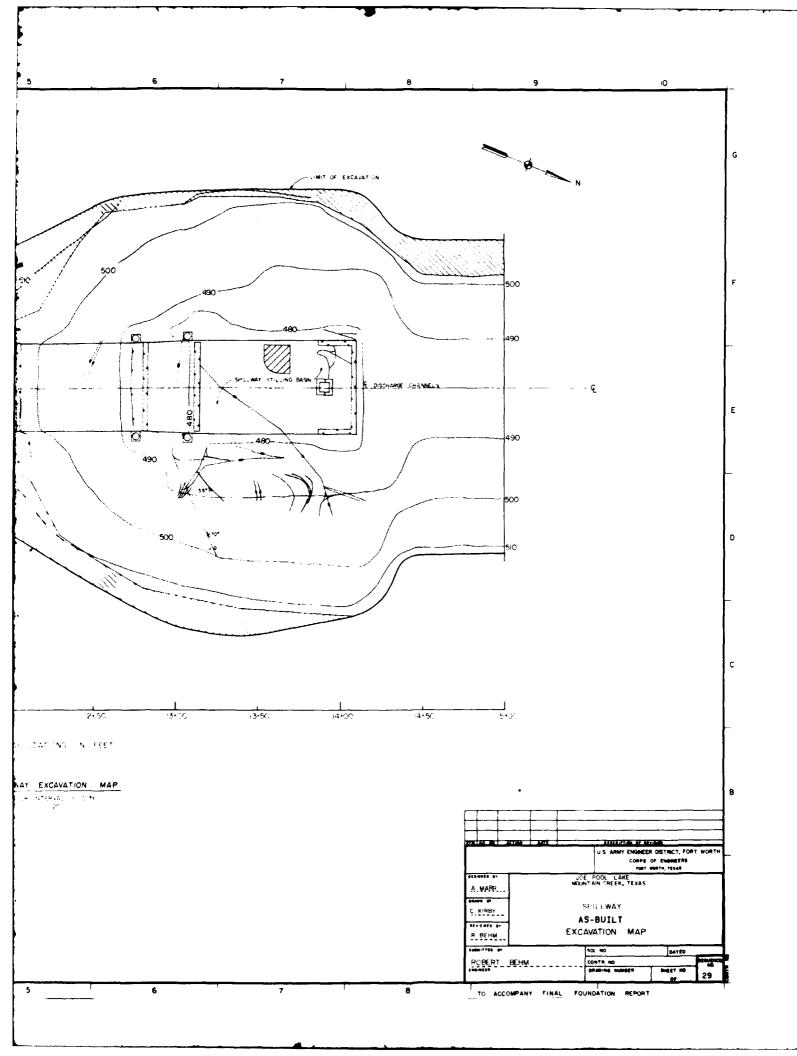


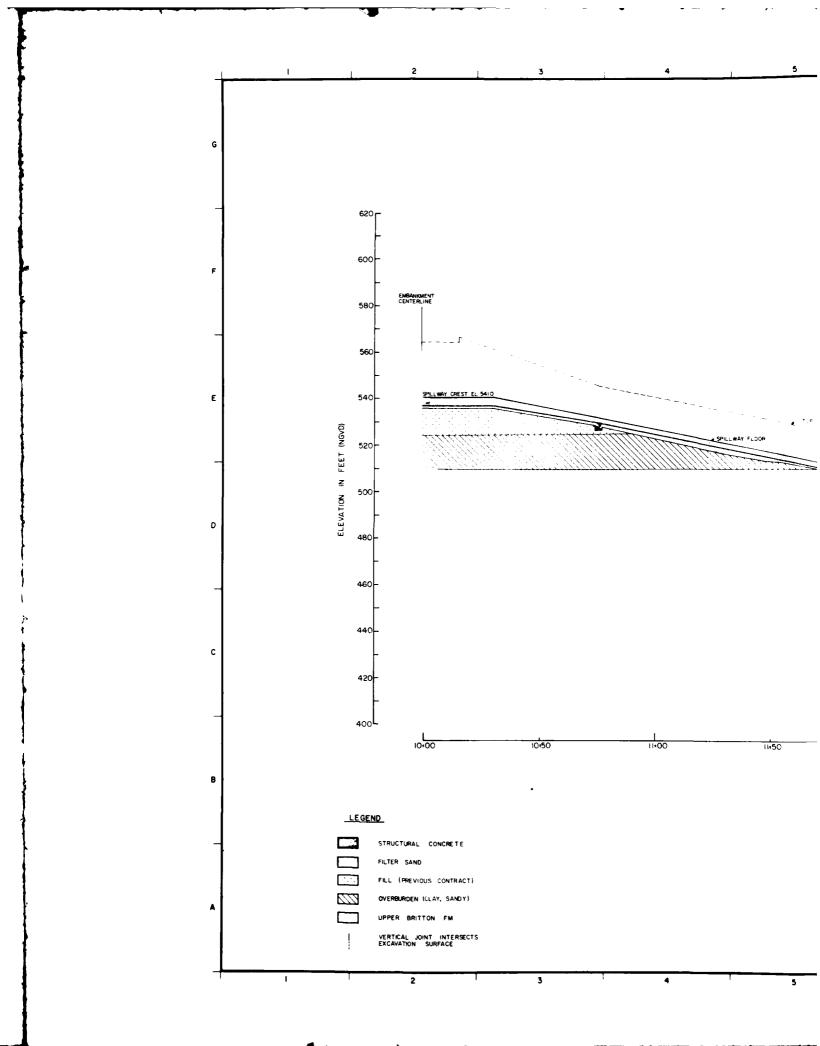


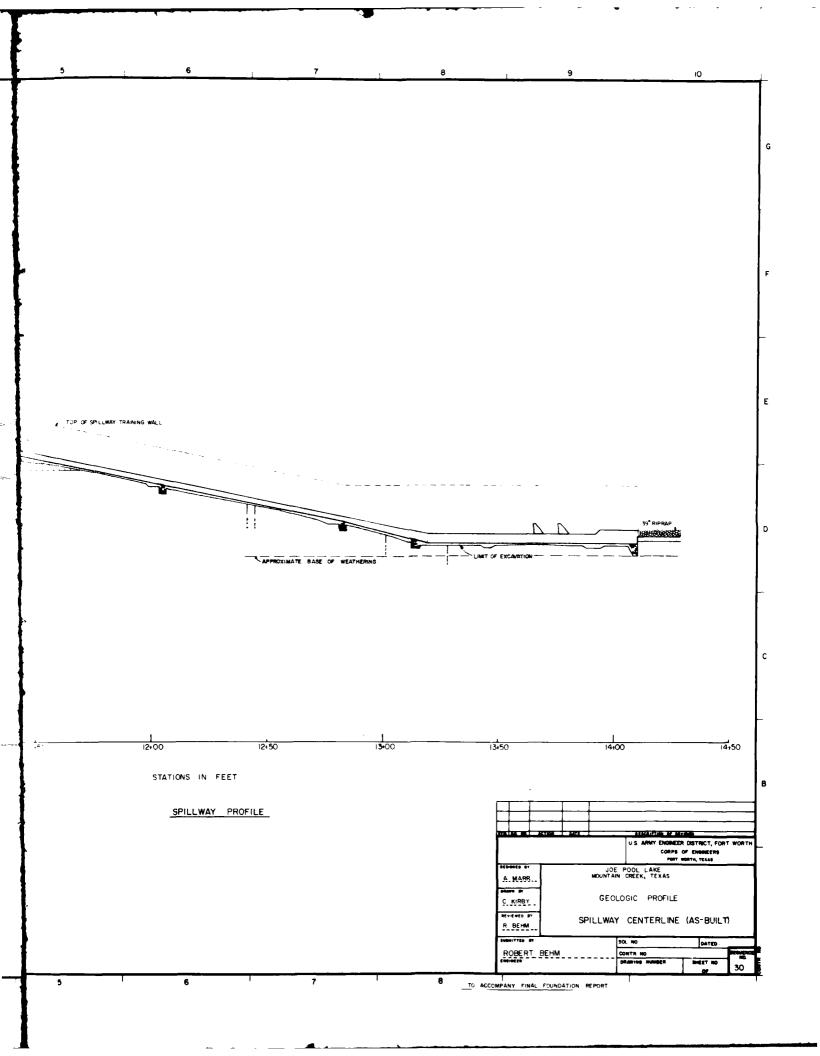
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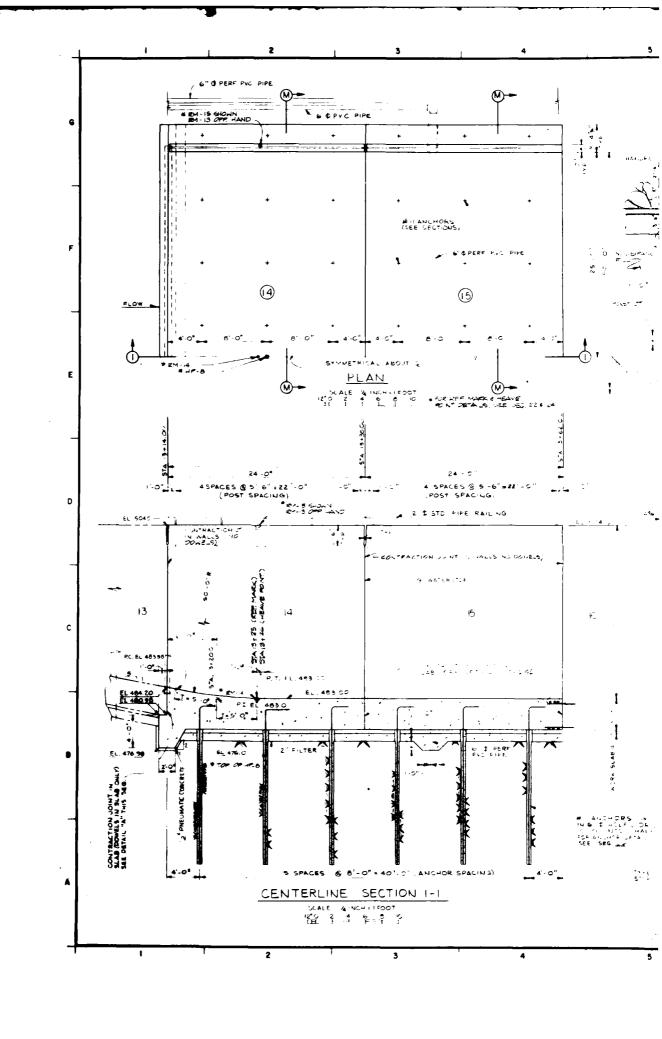


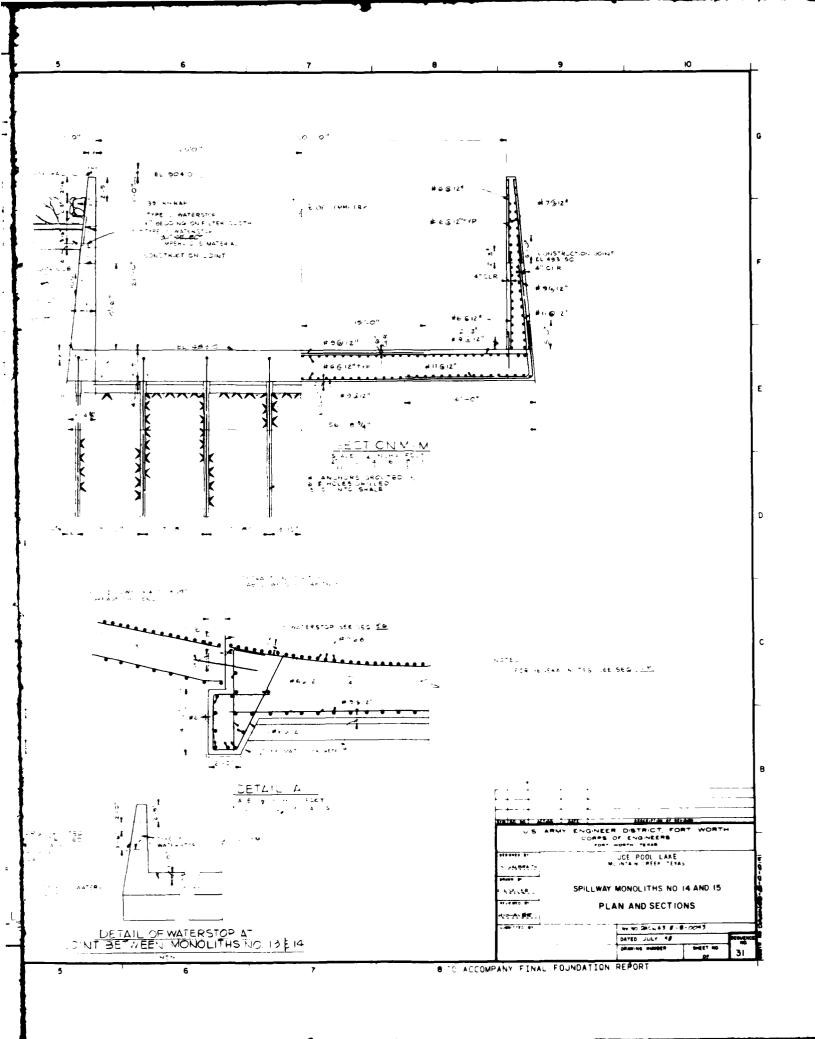


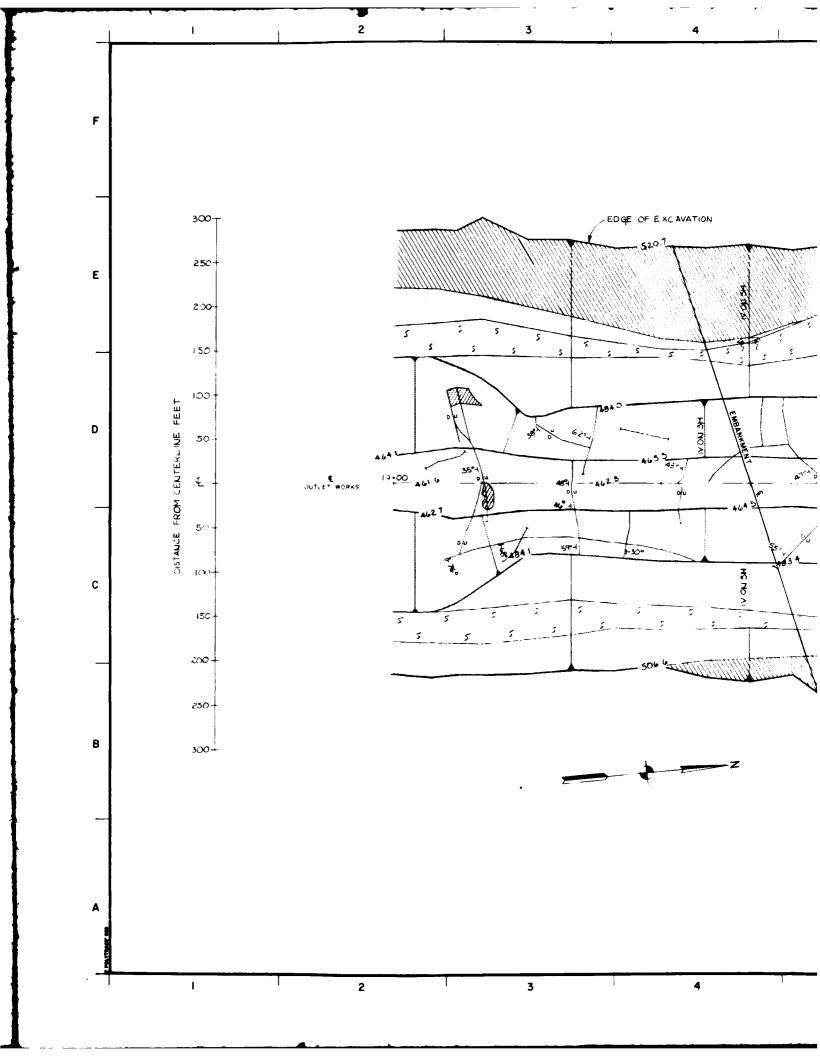


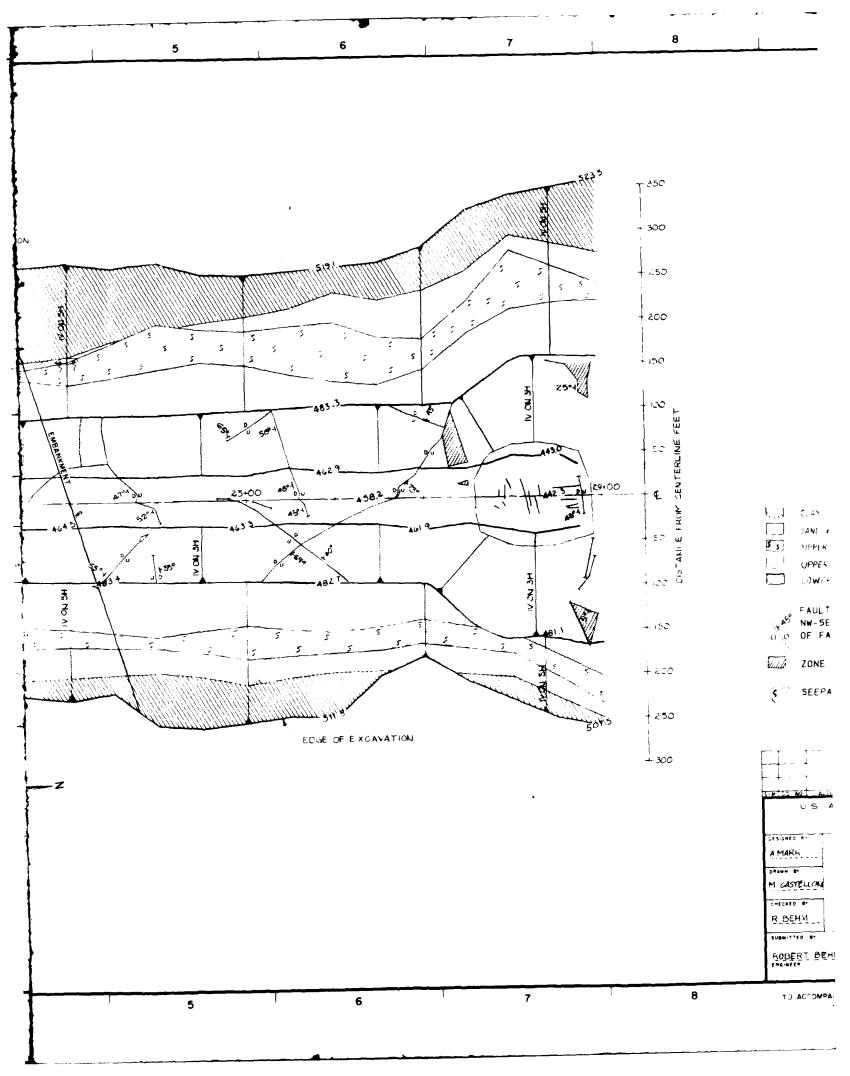


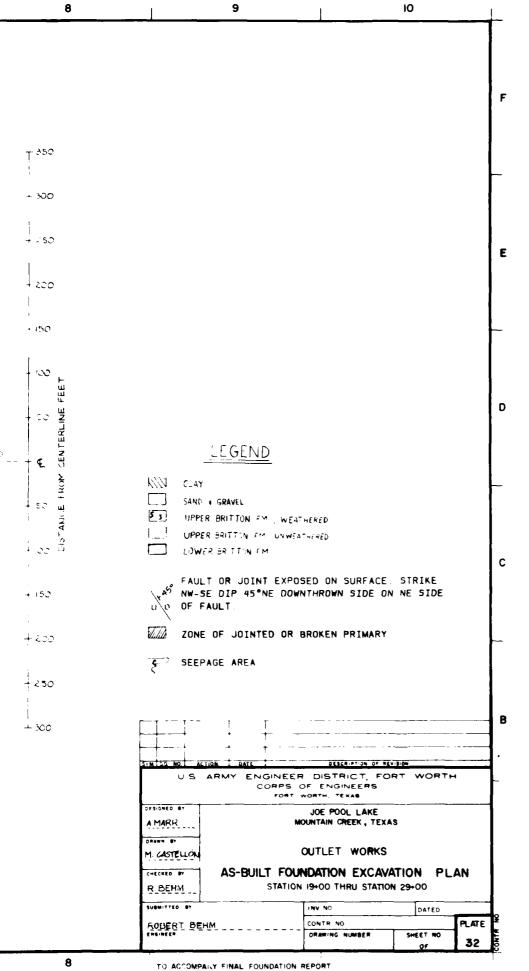












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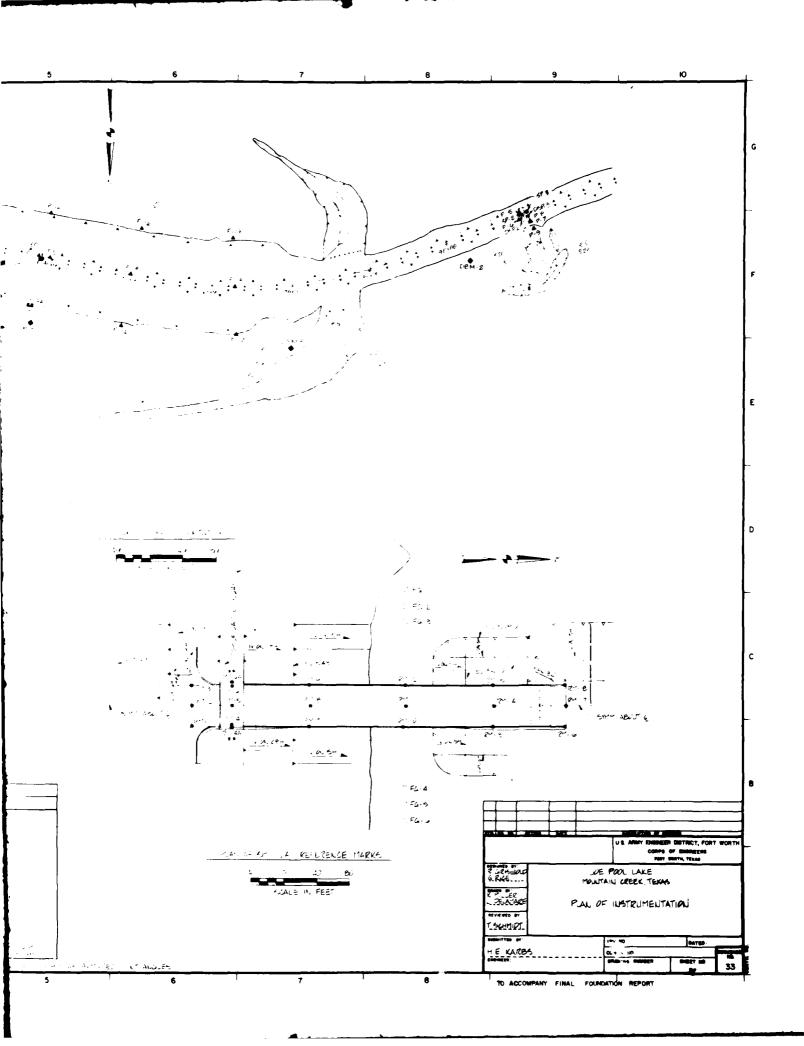
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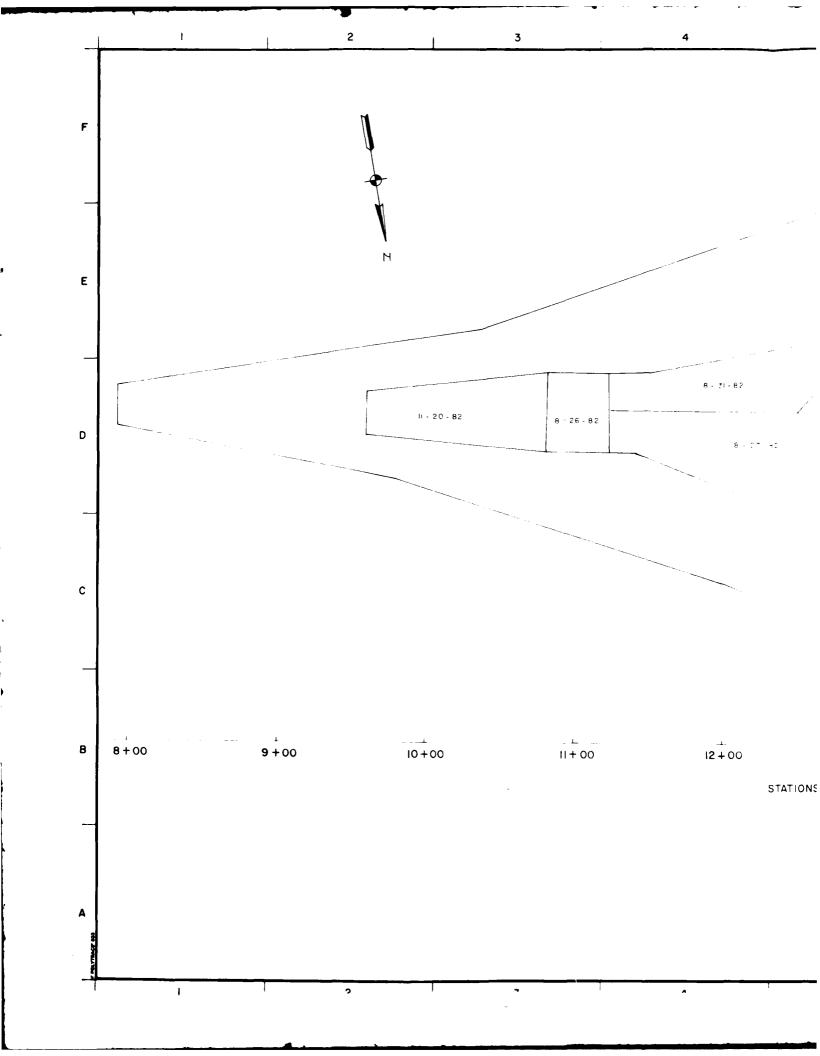
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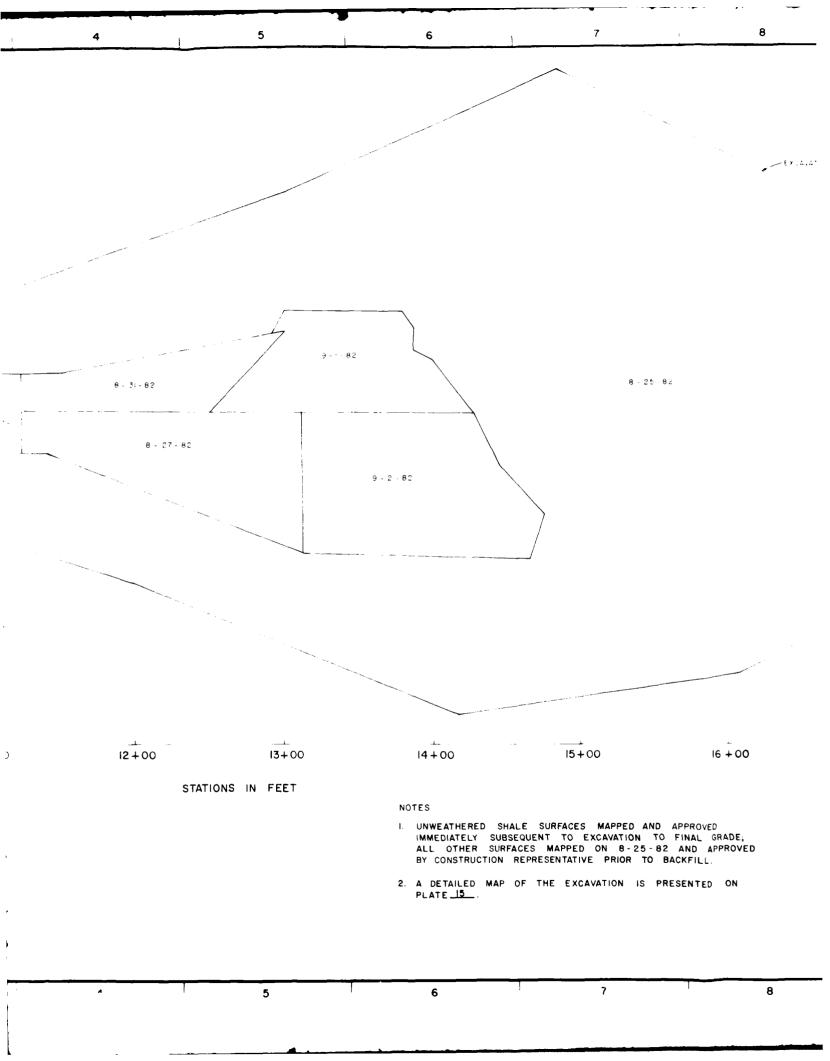
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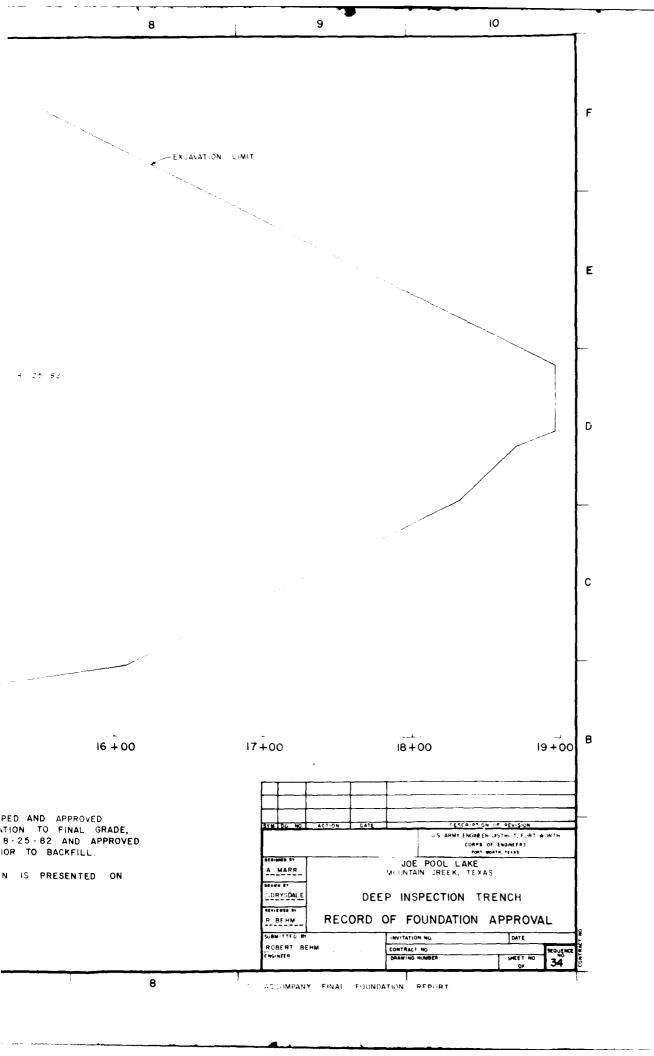
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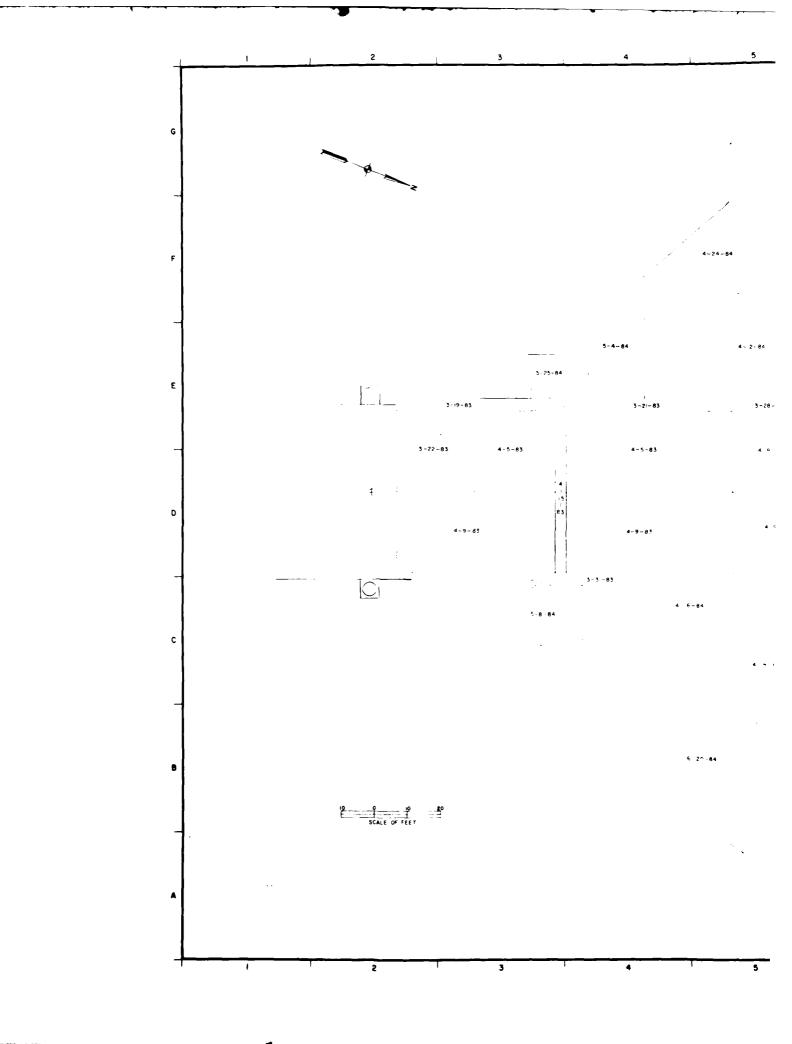
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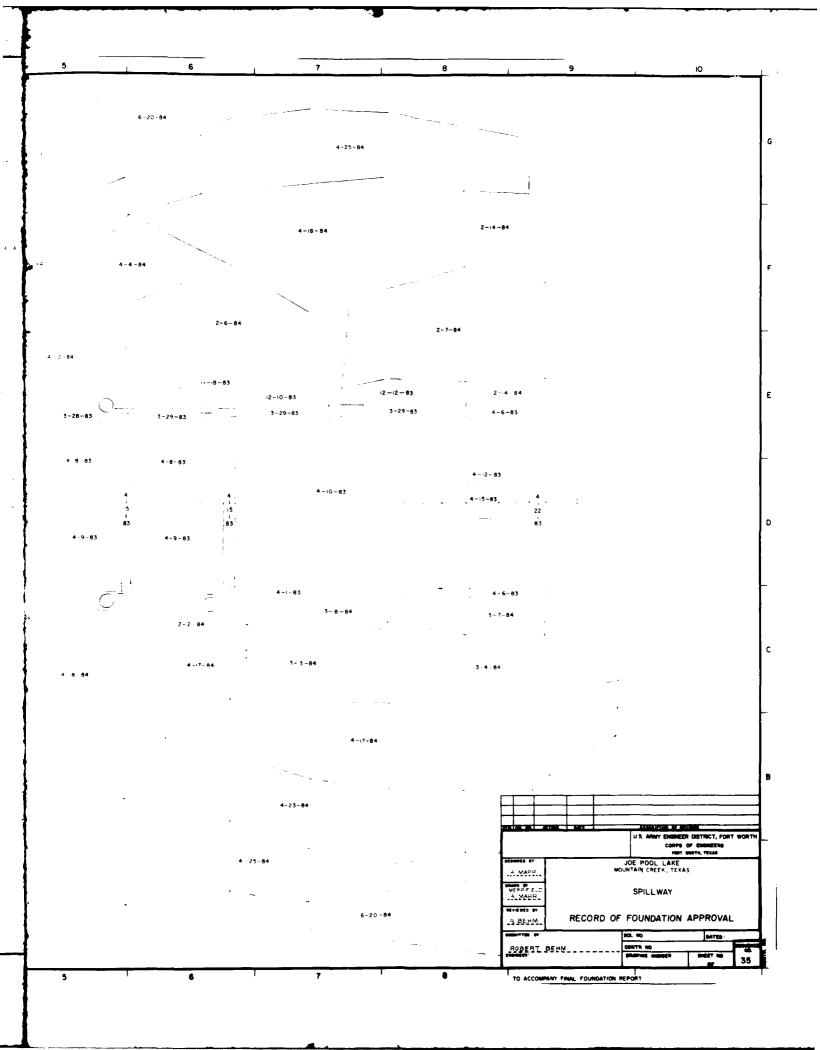


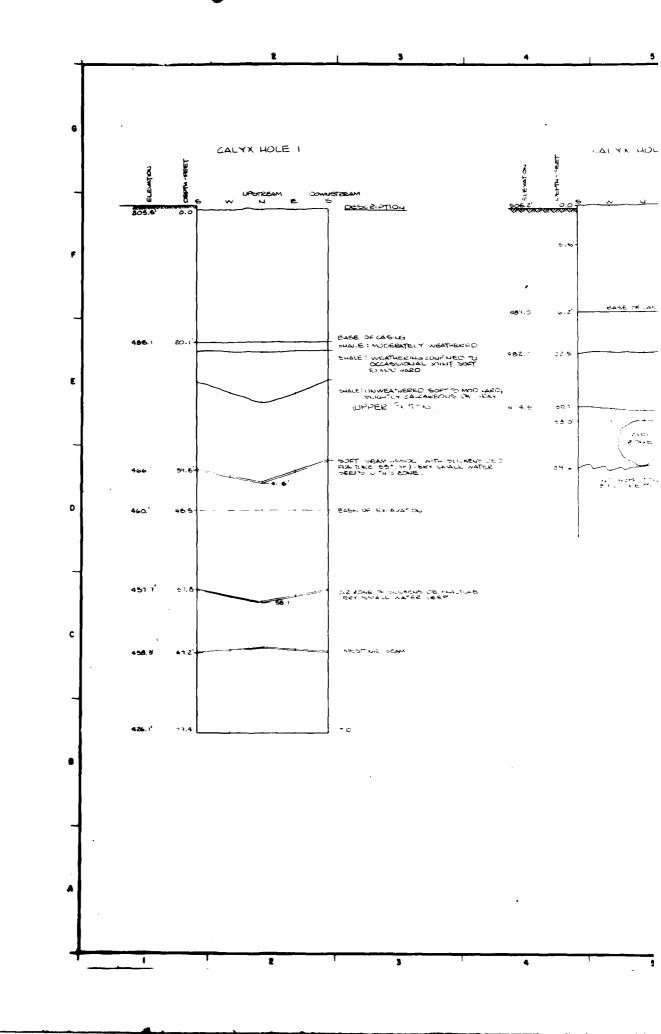


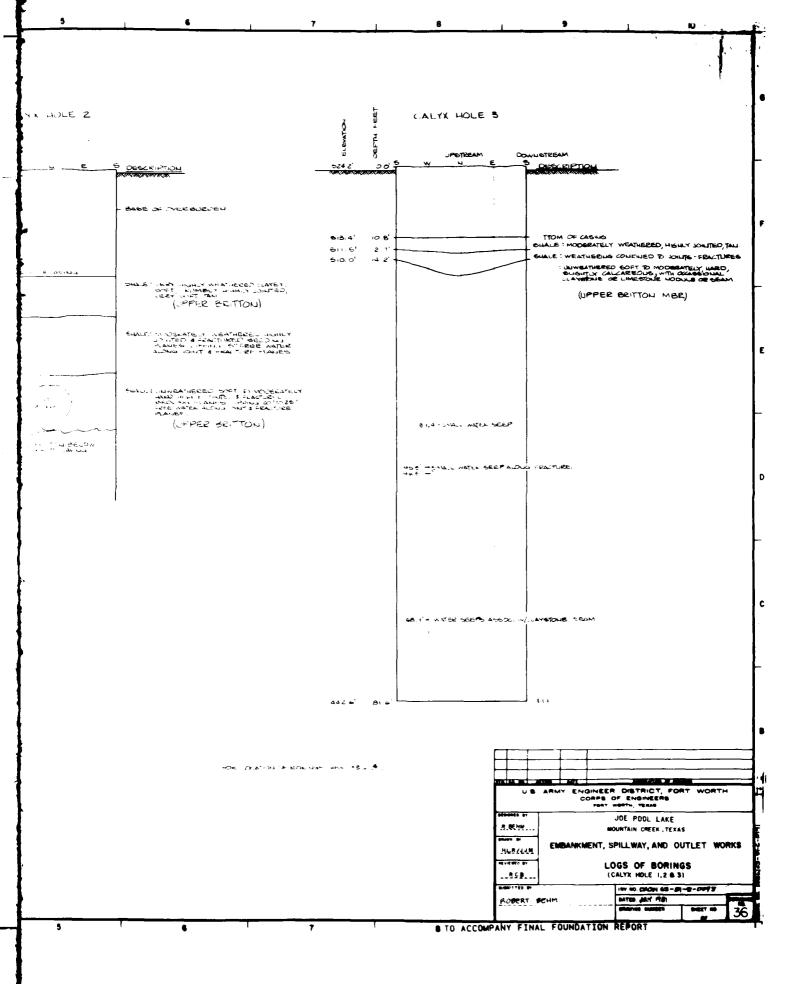


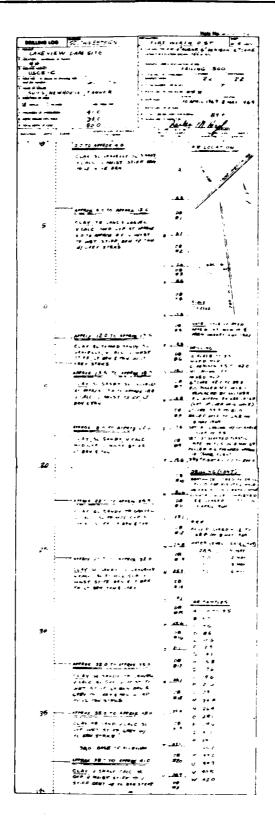






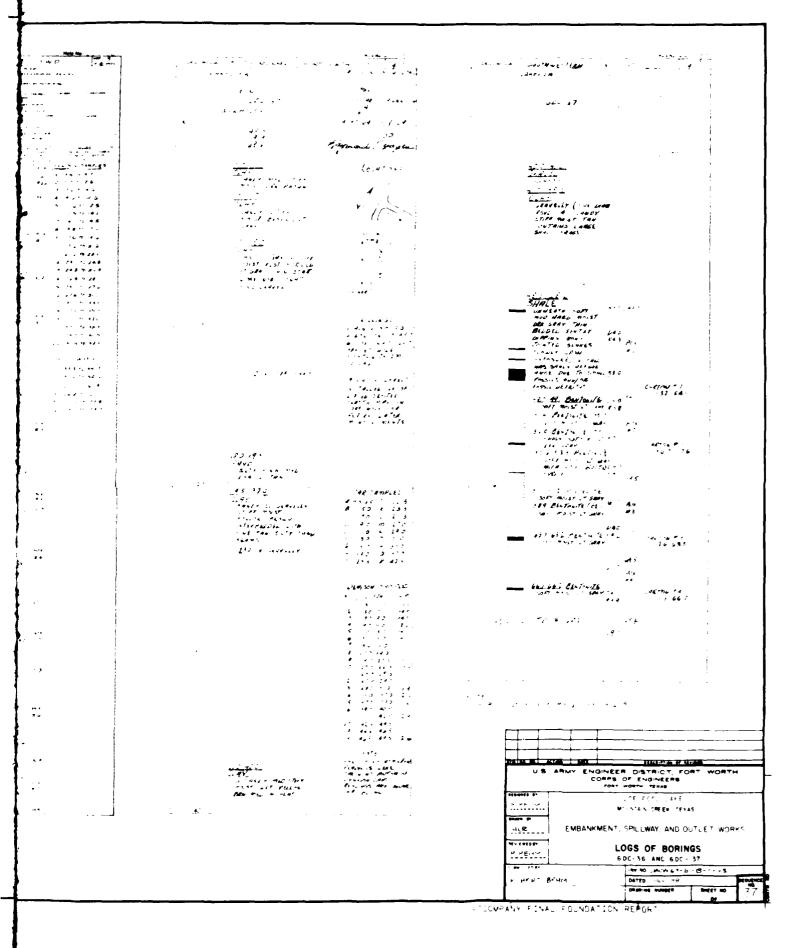






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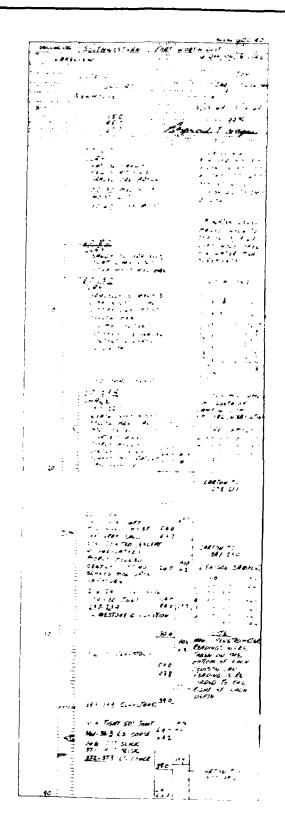
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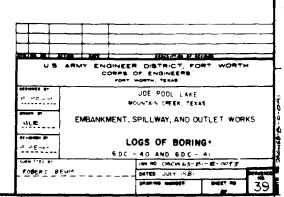
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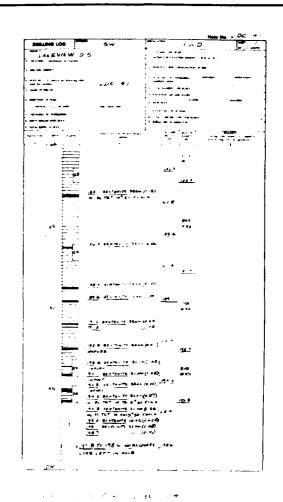
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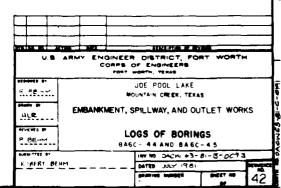
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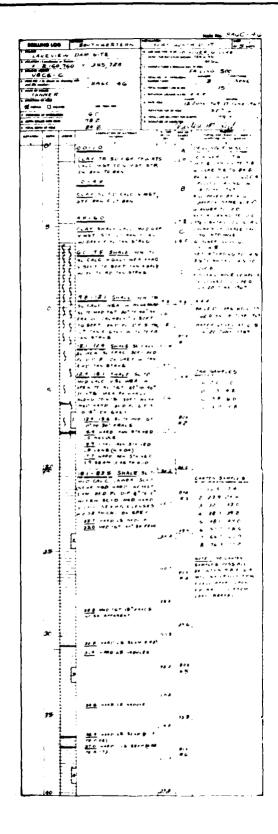
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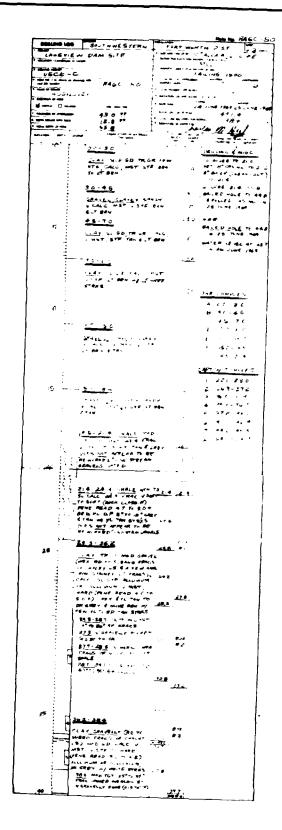
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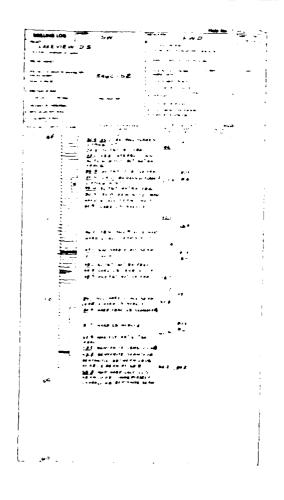
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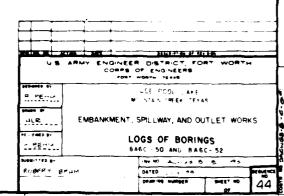


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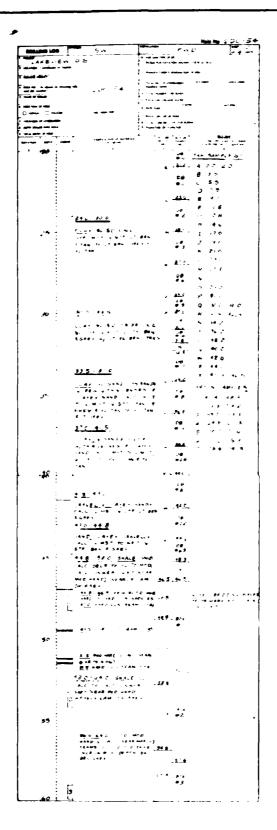
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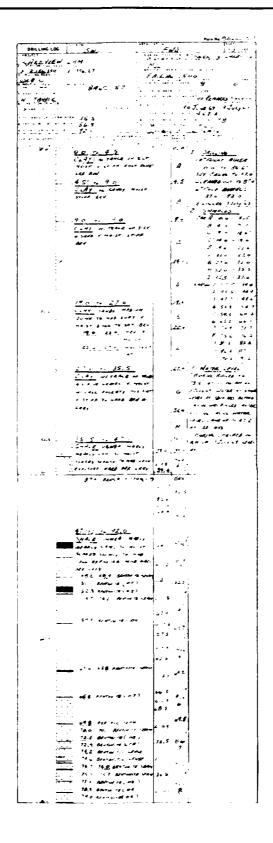
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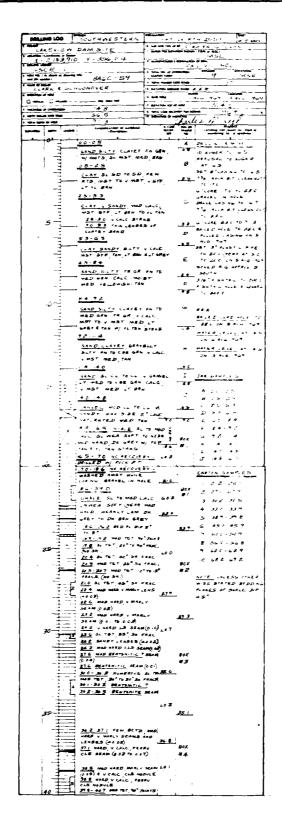
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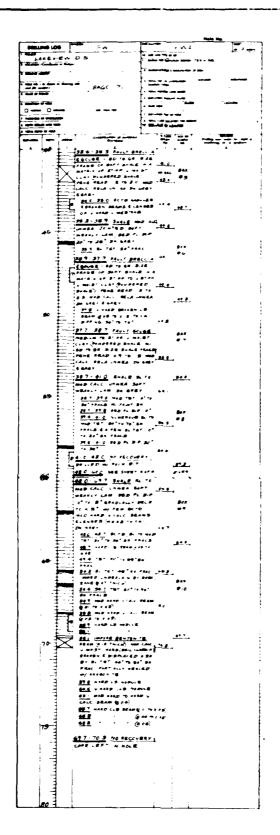
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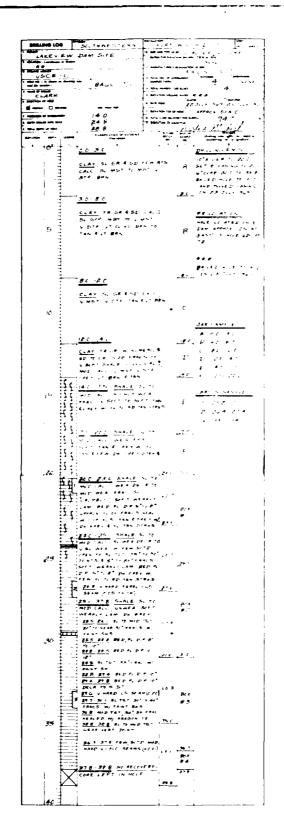
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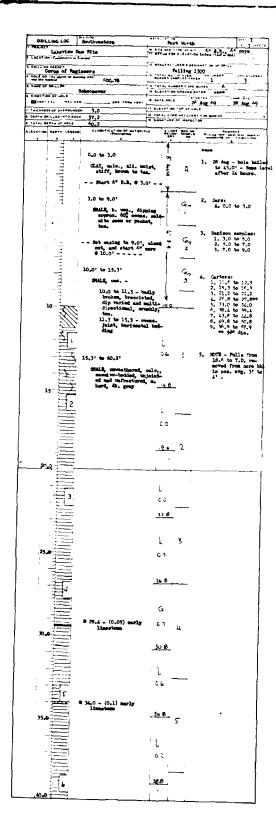
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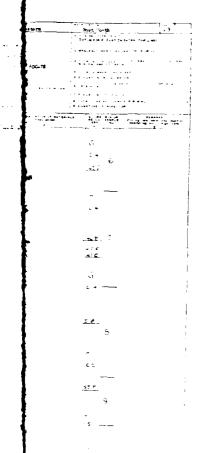
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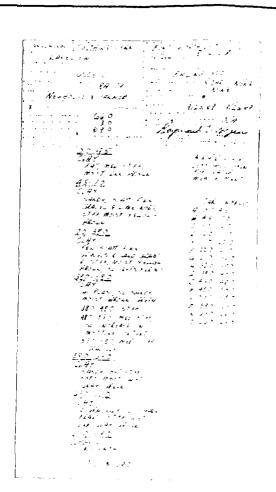
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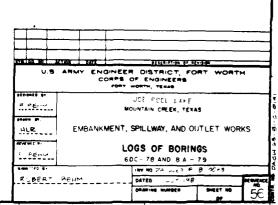
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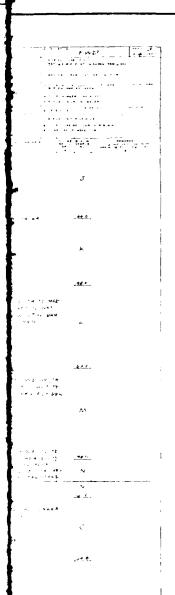


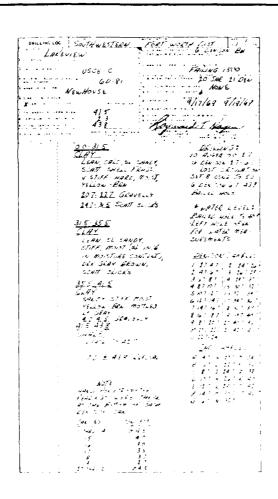


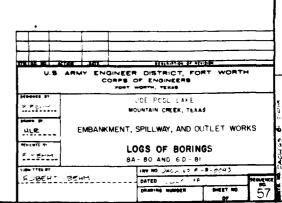
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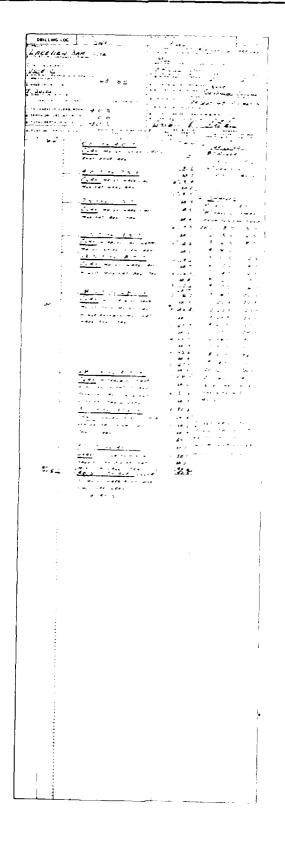


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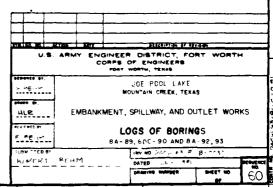
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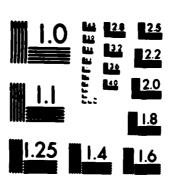
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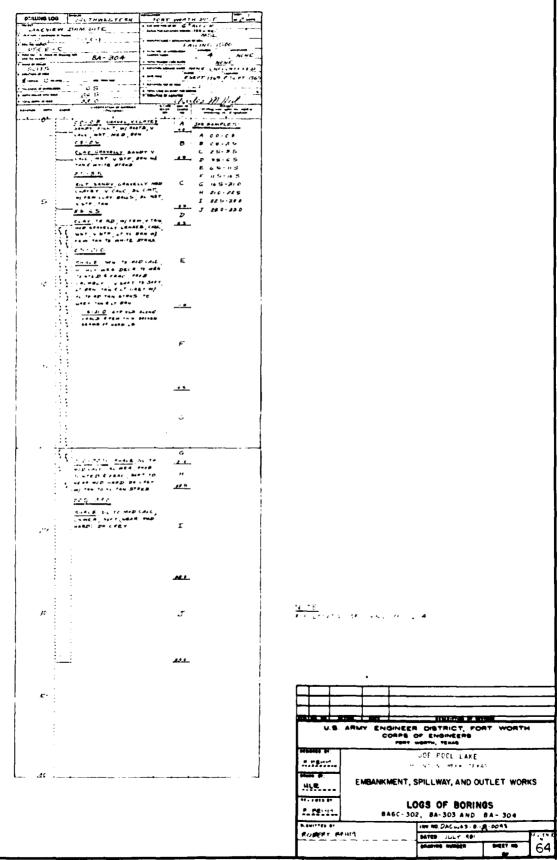
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Figure 7. Excavation slope being prepared for backfill. Right (north) side of right abutment deep inspection trench. 27 August 1982.



Figure 8. Excavation slope being prepared for backfill. Left (south) side of right abutment deep inspection trench. 31 August 1982.



Figure 9. Excavation slope being prepared for backfill. Left (south) side of right abutment deep inspection trench. 1 September 1982.



Figure 10. Excavation slope being prepared for backfill. Right (north) side of right abutment deep inspection trench. 2 September 1982.



Figure 11. Excavation slope being cut to final grade. 20 November 1982. Photo taken at £ right abutment deep inspection trench, station 10+50, looking west.



Figure 12. Excavation slope being cut to final grade. 20 November 1982. Photo taken near Lright abutment deep inspection trench, station 11+50, looking east.



Figure 13. Excavation in area of stream channel. (Embankment centerline station 54+50 to 61+00) January 1983. Note seepage areas in photo at center and lower right. Photo taken at embankment centerline station 54+00, looking west.



Figure 14. Excavation in area of stream channel. (Embankment center-line station 54+50 to 61+00) January 1983. Note seepage area left side of photo on downstream slope of trench. Photo taken at embankment center-line station 60+00, looking east.



Figure 15. Backfill compaction in area of stream channel, January 1983. Photo taken at embankment & station 60+00, looking south (upstream).



Figure 16. Embankment inspection trench ready for impervious backfill. 29 May 1980. Photo taken at station 36+00, looking east.



Figure 17. Embankment inspection trench ready for impervious backfill. 29 May 1980. Photo taken at station 43+00, looking west.



Figure 18. Embankment inspection trench ready for impervious backfill. 14 September 1984. Photo taken at station 51+50, looking east.



Figure 19. Embankment inspection trench ready for impervious backfill. 14 September 1984. Photo taken at station 53+50, looking east.



Figure 20. Embankment inspection trench being prepared for impervious backfill. 1 March 1983. Photo taken at station 61+00, looking east.



Figure 21. Embankment inspection trench ready for impervious backfill.

17 January 1983. Photo taken at station 65+00 looking at downstream slope.



Figure 22. Empairment inspection trench. Clayey gravel zone exposed in inspection trench along embankment centerline at station 71+0.



Figure 23. Embankment inspection trench ready for impervious backfill. 28 April 1983. Photo taken at station 71+25, looking east.



Figure 24. Embankment inspection trench ready for impervious backfill. 26 October 1983. Photo taken at station 85+00, looking east.

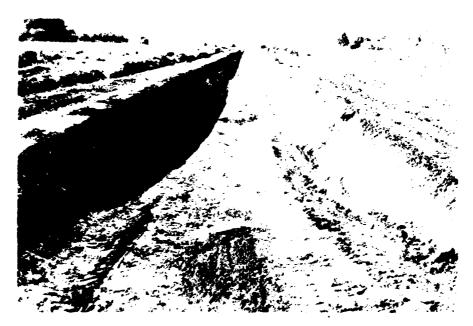


Figure 25. Embankment inspection trench ready for impervious backfill. 17 November 1983. Photo taken at station 88+00, looking west.



Figure 26. Embankment inspection trench ready for impervious backfill. 26 October 1983. Photo taken at station 88+50, looking east.



Figure 27. Embankment inspection trench ready for impervious backfill. 6 January 1981. Photo taken at station 95+00, looking west.

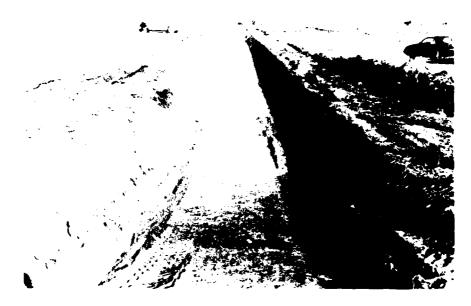


Figure 28. Embaukment inspection trench ready for impervious backfill. 17 November 1983. Photo taken at station 95+50, looking east.



Figure 29. Embankment inspection trench. Contact between previously placed impervious fill and natural ground exposed in side of inspection trench.



Figure 30. Embankment inspection trench ready for impervious backfill. 10 December 1983. Photo taken at station 130+00, looking west.



Figure 31. Embankment inspection trench ready for impervious backfill. 10 December 1983. Photo taken at station 132+00, looking west.

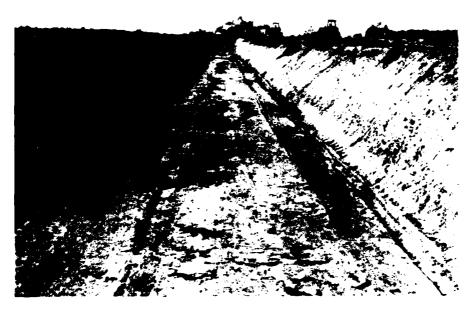


Figure 32. Embankment inspection trench ready for impervious backfill. 16 November 1983. Photo taken at station 147+00, looking west.

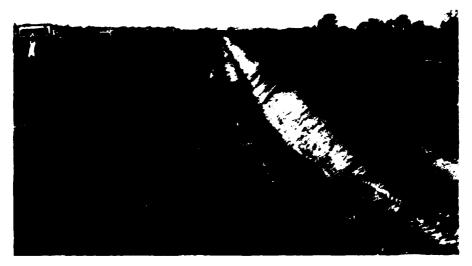


Figure 33. Embankment inspection trench ready for impervious backfill. 28 October 1983. Photo taken at station 150+50, looking west.



Figure 34. Embankment inspection trench ready for impervious backfill. 16 September 1983. Photo taken at station 172+00, looking east.



Figure 35. Embankment inspection trench ready for impervious backfill. 16 September 1986. Photo taken at station 186+00, looking east.



Figure 36. Embankment inspection trench ready for impervious backfill. 25 July 1983. Photo taken at station 191+00, looking west.



Figure 37. Embankment inspection trench ready for impervious backfill. 20 July 1983. Photo taken at station 209+50, looking east.



Figure 38. Embankment inspection trench ready for impervious backfill. 20 July 1983. Photo taken at station 210+00, looking west.

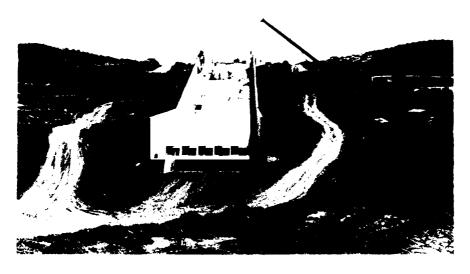


Figure 39. Spillway during construction. Spillway crest perched in the embankment.



Figure 40. Spillway foundation being prepared for backfill with sand filter blanket and protective slab. 9 April 1983.



Figure 41. Spillway wall footing excavation on right side of stilling basin ready for protective coating with pneumatic concrete. 6 April 1983. Spillway training wall footings in-place.

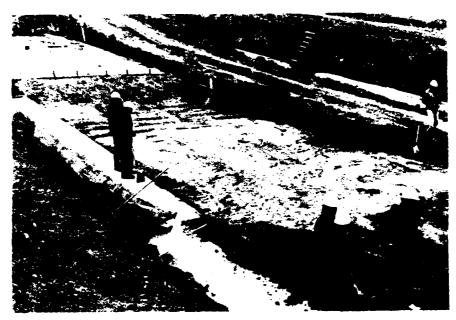


Figure 42. Spillway foundation being prepared for backfill with filter blanket and protective concrete. 5 April 1983.



Figure 43. Spillway foundation being prepared for backfill with filter blanket and protective concrete. 8 April 1983.



Figure 44. Spillway foundation ready for backfill with filter blanket and protective concrete. 9 April 1983.



Figure 45. Spillway foundation being prepared for backfill with filter blanket and protective concrete. 9 April 1983.



Figure 46. Spillway stilling basin foundation being prepared for backfill with filter blanket and protective concrete. 11 April 1983.

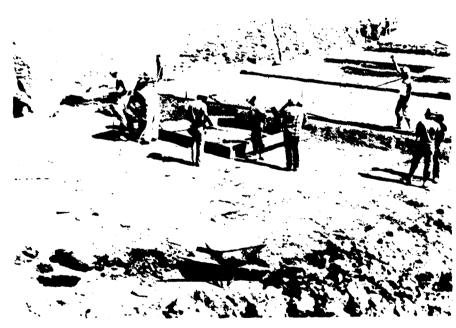


Figure 47. Spillway stilling basin foundation being prepared for backfill with filter blanket and protective concrete. 12 April 1983.



Figure 48. Spillway foundation. Key trench at spillway station 12+82 being prepared for backfill with reinforced concrete. 15 April 1983.



Figure 49. Spillway foundation. End sill excavation ready for protective coating with gunite.



Figure 50. Spillway foundation - end sill trench. Void space observed behind pneumatic concrete resulted in deterioration of clay shale. Pneumatic concrete less than $1\frac{1}{2}$ -inch required thickness.



Figure 51. Excavation adjacent to right spillway training wall being prepared for backfill with select impervious fill. 3 March 1984.



Figure 52. Foundation adjacent to right spillway training wall ready for backfill with select impervious fill. 3 March 1984.



Figure 53. Excavation adjacent to right spillway training wall being prepared for backfill with select impervious fill. 18 April 1984.



Figure 54. Foundation adjacent to right spillway training wall being prepared for backfill with select impervious fill. 18 April 1984.



Figure 55. Foundation adjacent to left spillway training wall ready for backfill with select impervious fill. 7 February 1984.

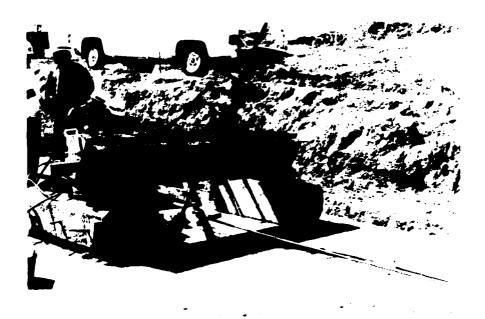


Figure 56. Foundation anchor pull-out test in progress. Test was conducted on 15 April 1983 at spillway station 11+70.



Figure 57. Drop structure constructed in diversion channel adjacent to spillway discharge channel. Photo looking east.



Figure 58. Drop structure foundation being prepared for backfill with protective concrete. 7 December 1982.

FINAL FOUNDATION REPORT JOE POOL LAKE

APPENDIX I

FOUNDATION ANCHOR PULL-OUT TEST DATA

Joe Pool Spillway - Anchor Pull-Out Test - 15 April 1983

Location of Test: Spillway Station 11+70 offset 20 ft left of center-line.

Description of Anchor: No. 11 rebar grouted in 6-inch diameter hole, 15 feet deep, at 59° from horizontal.

Results of Test:

	GAGE NO. 1			GAGE NO. 2		
				ACCUM		ACCUM
PSI	TONS	TIME	READING	MOVEMENT(IN.)	READ ING	MOVEMENT(IN.)
	0	1029	0.114	0	0.137	0
467	5	1029	0.129	0.015	0.152	0.015
467	5	1034	0.125	0.011	0.149	0.012
934	10	1035	0.151	0.037	0.177	0.040
934	10	1040	0.152	0.038	0.176	0.039
1457	15.6	1041	0.187	0.073	0.212	0.075
1457	15.6	1101	0.202	0.088	0.226	0.089
0	0	1101	0.129	0.015	0.153	0.016
0	0	1106	0.128	0.014	0.152	0.015
467	5	1106	0.163	0.049	0.189	0.052
467	5	1111	0.165	0.051	0.189	0.052
934	10	1111	0.186	0.072	0.210	0.073
934	10	1116	0.185	0.071	0.210	0.073
1401	15	1117	0.204	0.090	0.228	0.091
1401	15	1126	0.211	0.097	0.236	0.099
1868	20	1127	0.236	0.122	0.262	0.125
1868	20	1132	0.241	0.127	0.266	0.129
2335	25	1132	0.269	0.155	0.296	0.159
2335	25	1137	0.281	0.167	0.307	0.170
2802	30	1138	0.330	0.216	0.358	0.221
2802	30	1143	0.350	0.236	0.378	0.241
3269	35	1144	0.396	0.282	0.422	0.285
		red in w	ork slab			
3269	35	1150	0.426	0.312	0.452	0.315
3736	40	1151	0.500	0.386	0.526	0.389
3736	40	1156	0.543	0.429	0.570	0.433
4050	43.4	1157	0.770	0.656	0.793	0.656
4050	43.4	1200	0.778	0.664	0.802	0.665
2802	30	1201	0,745	0.631	0.768	0.631
2802	30	1206	0.746	0.632	0.770	0.633
1401	15	1206	0.684	0.570	0.706	0.569
1401	15	1211	0.683	0.569	0.704	0.567
0	0	1211	0.597	0.483	0.619	0.482
0	0	1214	0.574	0.460	0.597	0.460

END OF TEST

Joe Pool Drop Structure - Anchor Pull-Out Test - 17 January 1983

Location of Test: Drop structure Station 8+06.5 offset 12 ft left of centerline.

Description of Anchor: No. 11 rebar grouted in 6-inch diameter hole, 15 feet deep, at 60° from horizontal.

Results of Test:

PSI TONS 0	TIME 1250	READING	MOVEMENT(IN.)
0 0	1250		
U U		0	0
467 5	1251	0.012	0.012
934 10	1256	0.024	0.024
1457 15.6	1301	0.041	0.041
1457 15.6	1316	0.043	0.043
1868 20	1316	0.054	0.054
1868 20	1321	0.056	0.056
2802 30	1326	0.079	0.079
3269 35	1331	0.090	0.090
3736 40	1346	0.101	0.101
3736 40	1351	0.104	0.104
4203 45	1351	0.119	0.119
4203 45	1406	0.129	0.129
2802 30	1406	0.111	0.111
1457 15.6	1411	0.087	0.087
0 0	1426	0.050	0.050
0 0	1435	0.046	0.046
Reset gage to 0.000			
467 5	1435	0.011	0.057
467 5	1440	0.013	0.059
934 10	1440	0.025	0.071
934 10	1455	0.027	0.073
1457 15	1455	0.048	0.094
1457 15	1507	0.052	0.098
0 0	1507	0.009	0.055
1457 15	1508	0.049	0.095
1457 15	1509	0.051	0.097
2803 30	1509	0.111	0.157
4204 45	1510	0.180	0.226

END OF TEST

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